

Appendix A

Complex Number $s = a + jb$
 a, b are real
 $j = \sqrt{-1}$

RECTANGULAR FORM

Real part of s : $\text{Re}\{s\} = a$
 Imag. part of s : $\text{Im}\{s\} = b$

$$s = p e^{j\theta}$$

POLAR FORM

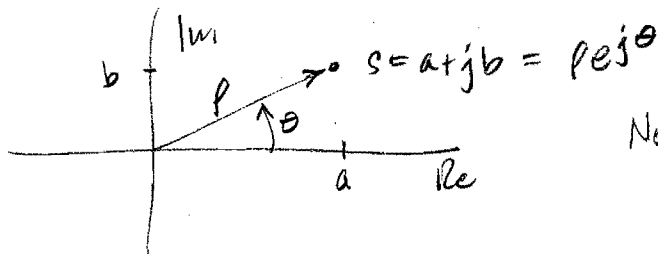
where $p \geq 0$ magnitude $\rightarrow p = |s|$
 θ angle (phase) $\rightarrow \theta = \angle s$

both p & θ are real numbers

Rectangular or polar form \rightarrow Complex plane representation:

$\text{Re}\{s\} = a \rightarrow$ real axis (HORIZONTAL)
 $\text{Im}\{s\} = b \rightarrow$ imag axis (VERTICAL)

$s = a + jb \sim$ vector representation



Note $|s| = |p e^{j\theta}|$

$$= |p| |e^{j\theta}| = |p| = p$$

since $p \geq 0$

EQUALITY: $s_1 = s_2$ iff $\text{Re}\{s_1\} = \text{Re}\{s_2\}$ AND $\text{Im}\{s_1\} = \text{Im}\{s_2\}$

alternatively,

$$s_1 = s_2 \text{ iff } p_1 = p_2 \text{ AND } \theta_1 = \theta_2$$

Conversion \leftrightarrow rectangular & polar coords

Euler's Formula $e^{j\theta} = \cos \theta + j \sin \theta$

\Downarrow note

$$e^{-j\theta} = \cos(-\theta) + j \sin(-\theta) \\ = \cos \theta - j \sin \theta$$

$$\therefore s = \rho e^{j\theta} = \rho (\cos \theta + j \sin \theta) \\ = a + jb$$

$$\Downarrow \\ \boxed{a = \rho \cos \theta \quad \& \quad b = \rho \sin \theta}$$

Furthermore, $a^2 = \rho^2 \cos^2 \theta$ & $b^2 = \rho^2 \sin^2 \theta$

$$\text{Since } \cos^2 \theta + \sin^2 \theta = 1 \rightarrow a^2 + b^2 = \rho^2 \cos^2 \theta + \rho^2 \sin^2 \theta \\ = \rho^2 (\cos^2 \theta + \sin^2 \theta) \\ = \rho^2$$

$$\boxed{\therefore \rho = \sqrt{a^2 + b^2}}$$

$$\text{also } \frac{b}{a} = \frac{\rho \sin \theta}{\rho \cos \theta} = \tan \theta \rightarrow \boxed{\theta = \tan^{-1}\left(\frac{b}{a}\right)}$$

in general,
$$\theta = \begin{cases} \tan^{-1}(b/a) & \text{when } a > 0 \\ \tan^{-1}(b/a) + 180^\circ & \text{when } a < 0 \end{cases}$$

Complex conjugate of $s \rightarrow \bar{s} = a - jb = \rho e^{-j\theta}$

Complex ADDITION $s_1 + s_2 = (a_1 + a_2) + j(b_1 + b_2)$

Polar domain preferred! $\left\{ \begin{array}{l} \text{Complex MULTIPLICATION } s_1 s_2 = (a_1 a_2 - b_1 b_2) + j(a_1 b_2 + a_2 b_1) \\ \text{Complex DIVISION } s_1 / s_2 = \frac{(a_1 a_2 + b_1 b_2) + j(-a_1 b_2 + a_2 b_1)}{a^2 + b^2} \end{array} \right.$

\uparrow
perform as $\frac{s_1}{s_2} \times \frac{\bar{s}_2}{\bar{s}_2} \dots \rightarrow$

CONTINUOUS-TIME
v.
DISCRETE-TIME

Signal: $x(t)$ real-valued (scalar-valued) fn of t .

↑
some signals defy concise mathematical description
- could be represented by sample values
 $\{x(t_0), x(t_1), \dots, x(t_N)\}$

Manipulation of signals \rightarrow Signal processing

Relationship b/w input and output \rightarrow Systems.

Systems, Signals and Models can be represented & analyzed
in time-domain or frequency domain

Continuous-Time Signals.

UNIT STEP FN. $u(t) = \begin{cases} 1 & t \geq 0 \\ 0 & t < 0 \end{cases}$

Notes:

$Ku(t) = \begin{cases} K & t \geq 0 \\ 0 & t < 0 \end{cases}$ and $x(t)u(t) = \begin{cases} x(t) & t \geq 0 \\ 0 & t < 0 \end{cases}$

UNIT-RAMP FN. $r(t) = tu(t) = \begin{cases} t & t \geq 0 \\ 0 & t < 0 \end{cases}$

Note: $r(t) = \int_{-\infty}^t u(\lambda) d\lambda$

UNIT IMPULSE FN $\delta(t) = 0 \quad t \neq 0$

↑ $\int_{-\epsilon}^{\epsilon} \delta(\lambda) d\lambda = 1$ for any real $\epsilon > 0$

delta fn / Dirac distribution

Note: $\delta(t)$ is NOT defined at $t=0$. also, $u(t) = \int_{-\infty}^t \delta(\lambda) d\lambda$ ↙ all $t, t \neq 0$

PERIODIC SIGNALS $x(t+T) = x(t) \quad -\infty < t < \infty$

↑
 $T \sim$ period (fixed, positive real number)

fundamental period is smallest value of
 \swarrow T for which equation holds.

Note: also periodic for integer multiples of T , i.e., $x(t+qT) = x(t)$ Sinusoids are periodic. $x(t) = A \cos(\omega t + \theta) \quad -\infty < t < \infty$

↓
 Note: $A \cos\left[\omega\left(t + \frac{2\pi}{\omega}\right) + \theta\right] = A \cos(\omega t + 2\pi + \theta)$
 $= A \cos(\omega t + \theta)$

$\therefore A \cos(\omega t + \theta)$
 is periodic w/ period $T = \frac{2\pi}{\omega}$

\swarrow
 $x(t) = A \cos(\omega t + \theta)$

$$x\left(t + \frac{2\pi}{\omega}\right) = A \cos\left(\omega\left(t + \frac{2\pi}{\omega}\right) + \theta\right) = A \cos(\omega t + 2\pi + \theta)$$

$$= A \cos(\omega t + \theta)$$

$$= x(t).$$

Note: $A \cos(\omega t - \pi/2) = A \sin(\omega t)$

Is the sum of two periodic signals periodic?

if $x_1(t)$ is periodic w/ period T_1
 & $x_2(t)$ is periodic w/ period T_2

then $x_1(t) + x_2(t)$ is periodic w/ period T

iff $\frac{T_1}{T_2} = \frac{q}{r}$ where q and r are integers.

in such a case, $T = rT_1 = qT_2$

skip

TIME-SHIFTED SIGNAL

if t_1 is positive real number $\rightarrow x(t-t_1)$ is $x(t)$ shifted RIGHT
by t_1 seconds

$\rightarrow x(t+t_1)$ is $x(t)$ shifted LEFT
by t_1 seconds.

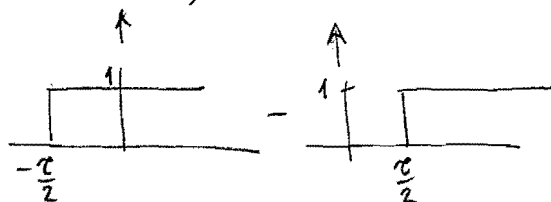
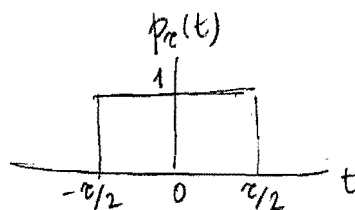
\uparrow
use $u(t)$ to demonstrate.

CONTINUOUS & PIECE-WISE CONTINUOUS SIGNALS

\uparrow (discontinuous at fixed point t_1 if $x(t_1^-) \neq x(t_1^+)$)
 \uparrow (finite or countably infinite # of discontinuities. (ex. pulse train))

Note: rectangular pulse fn.

$$p_{\tau}(t) = u\left(t + \frac{\tau}{2}\right) - u\left(t - \frac{\tau}{2}\right)$$



SIGNALS DEFINED INTERVAL-BY-INTERVAL

$$x(t) = \begin{cases} x_1(t) & t_1 \leq t \leq t_2 \rightarrow \text{interval defined by } u(t-t_1) - u(t-t_2) \\ x_2(t) & t_2 \leq t < t_3 \rightarrow \quad \quad \quad u(t-t_2) - u(t-t_3) \\ x_3(t) & t \geq t_3 \rightarrow \quad \quad \quad u(t-t_3) \end{cases}$$

$$\therefore x(t) = x_1(t) [u(t-t_1) - u(t-t_2)]$$

$$+ x_2(t) [u(t-t_2) - u(t-t_3)] + x_3 u(t-t_3)$$

$$= x_1 u(t-t_1) + [x_2(t) - x_1(t)] u(t-t_2) + [x_3(t) - x_2(t)] u(t-t_3)$$

DISCRETE-TIME SIGNALS.

$$x[n] \quad n \sim \text{integer valued}$$

↑ discrete points in time
 $t = nT \rightarrow n$

SAMPLING (UNIFORM)

$$x[n] = x(t) \big|_{t=nT} = x(nT)$$

$T \sim \text{sampling interval}$
(1/samp. freq.)

STEP FN. $u[n] = \begin{cases} 1 & n = 0, 1, 2, \dots \\ 0 & n = -1, -2, \dots \end{cases}$

RAMP FN. $r[n] = \begin{cases} n & n = 0, 1, 2, \dots \\ 0 & n = -1, -2, \dots \end{cases}$

$u[n] \& r[n]$ could
be generated by sampling
 $u(t) \& r(t)$ w/ sampling
interval, $T=1$

UNIT PULSE $\delta[n] = \begin{cases} 1 & n = 0 \\ 0 & n \neq 0 \end{cases}$

Note: unit pulse can NOT be generated by sampling $\delta(t)$

PERIODIC DISCRETE-TIME SIGNALS

$$x[n+r] = x[n] \quad \forall \text{ integers } n$$

↑ positive integer r

fundamental period - smallest value of r
for which $x[n+r] = x[n]$

Sinusoid - $x[n] = A \cos(\Omega n + \theta)$

$\Omega \sim \text{discrete-time frequency}$

$$x[n+r] = A \cos(\Omega n + \Omega r + \theta)$$

for $x[n] = x[n+r]$, Ωr must be multiple of 2π
i.e.,

$$\Omega r = 2\pi q \quad \text{for some integer } q$$

⇓

$$x[n] = x[n+r] \longrightarrow \text{if } \Omega = \frac{2\pi q}{r} \quad \text{for some positive integers } q \& r$$

clap

Note: for $x[n] = A \cos(\Omega n + \theta)$

↑
periodic iff $\Omega = 2\pi \frac{q}{r}$ where q & r
are positive integers!

RECTANGULAR PULSE

$$p_L[n] = \begin{cases} 1 & n = -\frac{(L-1)}{2}, \dots, -1, 0, 1, \dots, \frac{(L-1)}{2} \\ 0 & \text{all other } n \end{cases}$$

Note: according to this definition, L should be odd.

DIGITAL SIGNAL (as opposed to discrete-time signal)

Let $\{a_1, a_2, \dots, a_N\}$ be set of N real numbers

digital signal $x[n]$ is a discrete-time signal
whose values belong to the finite set $\{a_0, a_1, \dots, a_N\}$

DISCRETE-TIME SIGNAL - DISCRETE IN TIME
INFINITE POSSIBLE RANGE OF VALUES

DIGITAL SIGNAL - DISCRETE IN TIME
FINITE RANGE OF VALUES

Note: A sampled continuous-time signal is not necessarily a digital signal.

TIME SHIFTED SIGNAL

$x[n-q]$ q -step right shift of $x[n]$

$x[n+q]$ q -step left shift of $x[n]$

DISCRETE-TIME SIGNALS DEFINED INTERVAL-BY-INTERVAL

$$x[n] = \begin{cases} x_1[n] & n_1 \leq n < n_2 \\ x_2[n] & n_2 \leq n < n_3 \\ x_3[n] & n \geq n_3 \end{cases}$$

interval $n_1 \rightarrow n_2 \rightarrow u[n-n_1] - u[n-n_2]$
 u $n_2 \rightarrow n_3 \Rightarrow u[n-n_2] - u[n-n_3]$
 u $n \geq n_3 \rightarrow u[n-n_3]$

$$\begin{aligned} x[n] &= x_1[n] (u[n-n_1] - u[n-n_2]) + x_2[n] (u[n-n_2] - u[n-n_3]) \\ &\quad + x_3[n] u[n-n_3] \\ &= x_1[n] u[n-n_1] + (x_2[n] - x_1[n]) u[n-n_2] \\ &\quad + (x_3[n] - x_2[n]) u[n-n_3] \end{aligned}$$

READ § 1.4 - Examples of Systems.

BASIC SYSTEM PROPERTIES.

CAUSALITY (nonanticipatory)

if for any time t_1 , the output response $y(t_1)$ at time t_1 , resulting from input $x(t)$ does not depend on values of the input $x(t)$ for $t > t_1$.

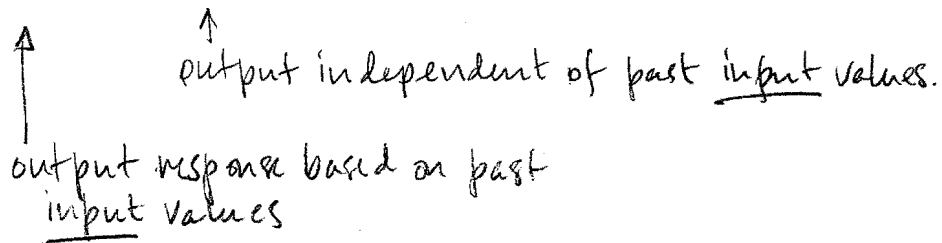
↑
current output not a fn of future input

or
 no output prior to applied input

Note:

off-line or non real-time processing may be NONCAUSAL.

MEMORY VS. MEMORYLESS



9-8-03 LINEARITY is $f(a_1 x_1(t)) + f(a_2 x_2(t)) = f(a_1 x_1(t) + a_2 x_2(t))$?
 given inputs $x_1(t) \neq x_2(t)$
 ↓ ↓
 w/ corresponding $y_1(t) \neq y_2(t)$
 outputs

↑ test for LINEARITY

and given scalars a_1 and a_2 , system is linear iff.

$$\underbrace{a_1 x_1(t) + a_2 x_2(t)}_{\text{aggregate input}} \longrightarrow \underbrace{a_1 y_1(t) + a_2 y_2(t)}_{\text{aggregate output}}$$

(assuming no initial energy in system)

Note: Nonlinear systems are FREQUENTLY approximated by linear ones

TIME INVARIANCE is $y(t-t_1) = f(x(t-t_1))$? test for TIME INVARIANCE

time shift in input \longrightarrow time shift in output

i.e. if $x(t) \rightarrow y(t)$ does $x(t) \rightarrow x(t-t_1)$
 and $x(t-t_1) \rightarrow y(t-t_1) \rightarrow$ precipitate $y(t) \rightarrow y(t-t_1)$?
 \longrightarrow TIME INVARIANT.

Likewise for discrete-time case, shift in input $x[n-n_1]$ yields corresponding shift in output $y[n-n_1]$

Eigenvalues of LTI systems are complex exponentials
 ($e^{j\omega t}$, thus, sinusoids)

LINEAR I/O DIFF EQ W/ CONSTANT COEFFICIENTS.

↑ continuous-time

$$y^{(N)}(t) + \sum_{i=0}^{N-1} a_i y^{(i)}(t) = \sum_{i=0}^M b_i x^{(i)}(t)$$

where $y^{(i)}(t) = \frac{d^i}{dt^i} [y(t)]$

$$\{a_0, a_1, \dots, a_{N-1}, b_0, b_1, \dots, b_M\} \in \mathbb{R} \text{ constants.}$$

From § 1.5 p.45

→ Diff. Eq. w/ constant coefficients → ATITo solve Diff Eq, need initial conditions for derivatives,
i.e.,

$$y(0), y^{(1)}(0), \dots, y^{(N-1)}(0) \text{ or at time } 0^-$$

1st ORDER DIFF EQ //

$$\frac{dy(t)}{dt} + ay(t) = bx(t)$$

Solution //

$$y(t) = e^{-at} y(0) + \int_0^t e^{-a(t-\lambda)} b x(\lambda) d\lambda$$

$t \geq 0$

Note: or time 0^- & need to know $y(0)$
assuming $x(t)$ applied for $t \geq 0$

FYI, if given

$$\frac{dy(t)}{dt} + ay(t) = b_1 \frac{dx(t)}{dt} + b_0 x(t)$$

⇓

Solution //

$$y(t) = e^{-at} [y(0) - b_1 x(0)] + \int_0^t e^{-a(t-\lambda)} (b_0 - ab_1) x(\lambda) d\lambda + b_1 x(t)$$

Note: or time 0^-
& need $y(0)$ & $x(0)$

 $t \geq 0$

EX. / 2.1 (a) $\frac{dy(t)}{dt} - 2y(t) = x(t)$ $x(t) = u(t)$
 $\uparrow a = -2$ $\uparrow b = 1$ $y(0) = 1$

$$y(t) = e^{-(-2)t} \overset{y(0)}{\cancel{y(0)}} + \int_0^t e^{-(-2)(t-\lambda)} (1) \overset{1}{\cancel{x(\lambda)}} d\lambda \quad t \geq 0$$

$$= e^{2t} + e^{2t} \int_0^t e^{-2\lambda} d\lambda$$

$$= e^{2t} + e^{2t} \left(\frac{1}{-2} \right) [e^{-2t} - 1]$$

$$= e^{2t} + \frac{1}{2} e^{2t} - \frac{1}{2}$$

$$= \frac{3}{2} e^{2t} - \frac{1}{2} \quad t \geq 0$$

EX. / 2.1 (d) $\frac{dy(t)}{dt} + 10y(t) = 2x(t)$ $x(t) = e^{4t}u(t)$
 $\uparrow a = 10$ $\uparrow b = 2$ $y(0) = 0$

$$y(t) = e^{-10t} \overset{y(0)}{\cancel{y(0)}} + \int_0^t e^{-10(t-\lambda)} (2) \overset{e^{4\lambda}}{\cancel{x(\lambda)}} d\lambda$$

$$= 2e^{-10t} \int_0^t e^{10\lambda} \cdot e^{4\lambda} d\lambda$$

$$= 2e^{-10t} \int_0^t e^{14\lambda} d\lambda$$

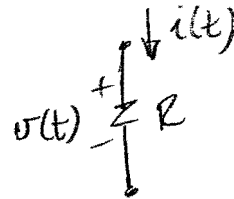
$$= 2e^{-10t} \cdot \frac{1}{14} [e^{14t} - 1]$$

$$= \frac{1}{7} e^{4t} - \frac{1}{7} e^{-10t} \quad t \geq 0$$

SYSTEM MODELING - ELECTRIC CKTS.

Resistor

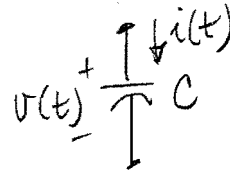
$$v(t) = R i(t)$$



Capacitor

$$\frac{dv(t)}{dt} = \frac{1}{C} i(t)$$

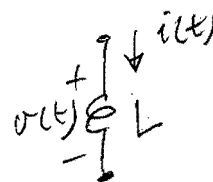
$$\nleftrightarrow v(t) = \frac{1}{C} \int_{-\infty}^t i(\lambda) d\lambda$$



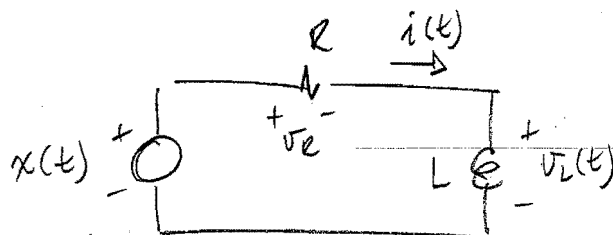
Inductor

$$v(t) = L \frac{di(t)}{dt}$$

$$\nleftrightarrow i(t) = \frac{1}{L} \int_{-\infty}^t v(\lambda) d\lambda$$

KVL $\rightarrow \sum \text{voltage drops} = \sum \text{adds.}$ KCL $\rightarrow \sum i \text{ into node} = 0.$

EX. / 2.8

I/O Eq b/w $x(t)$ & $i(t)$

$$v_R(t) = R i(t)$$

$$v_L(t) = L \frac{di(t)}{dt}$$

$$x(t) = R i(t) + L \frac{di(t)}{dt}$$

$$\left. \begin{aligned} x(t) &= u(t) \\ a &= \frac{R}{L}, b = \frac{1}{L} \end{aligned} \right\} \rightarrow i(t) =$$

$$\Rightarrow \frac{di(t)}{dt} + \frac{R}{L} i(t) = \frac{1}{L} x(t)$$

$$i(t) = e^{-\frac{R}{L}t} i(0) + \int_0^t e^{-\frac{R}{L}(t-\lambda)} \left(\frac{1}{L}\right) d\lambda$$

EX. / 2.8 (cont'd)

$$\begin{aligned}
 i(t) &= e^{-\frac{R}{L}t} i(0) + \frac{1}{L} e^{-\frac{R}{L}t} \int_0^t e^{\frac{R}{L}\lambda} d\lambda \\
 &= e^{-\frac{R}{L}t} i(0) + \frac{1}{L} e^{-\frac{R}{L}t} \cdot \frac{L}{R} [e^{\frac{R}{L}t} - 1] \\
 &= e^{-\frac{R}{L}t} i(0) + \frac{1}{R} [1 - e^{-\frac{R}{L}t}] \quad t \geq 0
 \end{aligned}$$

$$\begin{aligned}
 v_L(t) &= L \frac{di(t)}{dt} \\
 &= L \frac{d}{dt} \left[\right] \\
 &= L \cdot \left(-\frac{R}{L}\right) e^{-\frac{R}{L}t} i(0) + L \cdot \frac{1}{R} \cdot -\left(-\frac{R}{L}\right) e^{-\frac{R}{L}t} \\
 &= -R e^{-\frac{R}{L}t} i(0) + e^{-\frac{R}{L}t} \quad t \geq 0
 \end{aligned}$$

if $i(0) = 0$

$$\rightarrow v_L(t) = e^{-\frac{R}{L}t} \quad t \geq 0$$

ALTERNATIVELY

(a) I/O DIFF EQ w/ $v_L(t) \neq x(t)$

$$v_L(t) = L \frac{di(t)}{dt} \neq v_R(t) = R i(t)$$

 \Downarrow

$$\begin{aligned}
 x(t) &= R i(t) + \underbrace{L \frac{di(t)}{dt}}_{v_L(t)} \xrightarrow{d/dt} \frac{dx(t)}{dt} = R \frac{di(t)}{dt} + \frac{dv_L(t)}{dt} \\
 &= \underbrace{\frac{R}{L} v_L(t)}_{\text{}} + \frac{dv_L(t)}{dt}
 \end{aligned}$$

$$\therefore \frac{dv_L(t)}{dt} + \frac{R}{L} v_L(t) = \frac{dx(t)}{dt}$$

(b)

$$\text{if } x(t) = u(t) \rightarrow \frac{dx(t)}{dt} = \delta(t) \Rightarrow \frac{dv_L(t)}{dt} + \frac{R}{L} v_L(t) = \delta(t)$$

OVER \rightarrow

$$\begin{aligned}
 \therefore v_L(t) &= e^{-\frac{R}{L}t} v_L(0) + \int_0^t e^{-\frac{R}{L}(t-\lambda)} (1) \delta(\lambda) d\lambda \\
 &= e^{-\frac{R}{L}t} v_L(0) + e^{-\frac{R}{L}t} \cdot \left[e^{-\frac{R}{L}(t-0)} \right]_0^1 \\
 &= e^{-\frac{R}{L}t} v_L(0) + e^{-\frac{R}{L}t} \quad t \geq 0
 \end{aligned}$$

if $v_L(0) = 0 \rightarrow v_L(t) = e^{-\frac{R}{L}t} \quad t \geq 0$ same as previous answer.

(c) $v_L(0) = v_0 \neq x(t) = 1 \quad t \geq 0$

$$v_L(t) = e^{-\frac{R}{L}t} [1 + v_0] \quad t \geq 0$$

(d) $v_L(0) = 0 \neq x(t) = 1 + \frac{R}{L}t \quad t \geq 0$

$$\downarrow$$

$$\frac{dx(t)}{dt} = \delta(t) + \frac{R}{L}u(t)$$

$$\therefore v_L(t) = e^{-\frac{R}{L}t} \cancel{v_L(0)}^0 + \int_0^t e^{-\frac{R}{L}(t-\lambda)} \left[\delta(\lambda) + \frac{R}{L}u(\lambda) \right] d\lambda$$

$$= e^{-\frac{R}{L}t} + \frac{R}{L} \left(-\frac{1}{\frac{R}{L}} \right) e^{-\frac{R}{L}t} \left[e^{-\frac{R}{L}(t-t)} - 1 \right]$$

$$= e^{-\frac{R}{L}t} - e^{-\frac{R}{L}t} + 1$$

$$v_L(t) = 1 \quad t \geq 0$$

9-10-03 Ch 2 - System Definition

LINEAR I/O DIFFERENCE EQ w/ CONSTANT COEFFICIENTS

$$y[n] + \sum_{i=1}^N a_i y[n-i] = \sum_{i=0}^M b_i x[n-i]$$

where $\{a_1, a_2, \dots, a_N, b_0, b_1, \dots, b_M\} \in \mathbb{R}$ constants

Note: from § 1.5 p. 45, constant coefficients \rightarrow LTI

$$\text{If } y[n] = -\sum_{i=1}^N a_i y[n-i] + \sum_{i=0}^M b_i x[n-i]$$

has any $a_i \neq 0 \rightarrow$ Recursive sol'n (requires N previous values $\{y[n-1], \dots, y[n-N]\}$)

if all $a_i = 0$ for $i=1, \dots, N \rightarrow$ Nonrecursive

\Downarrow

$$y[n] = \sum_{i=0}^M b_i x[n-i]$$

9-15-03

FIRST ORDER LINEAR DIFFERENCE EQUATION

$$y[n] = -a y[n-1] + b x[n] \quad n=1, 2, \dots$$

w/ initial condition $y[0]$

\Downarrow

$$n=1 \quad y[1] = -a y[0] + b x[1]$$

$$n=2 \quad y[2] = -a y[1] + b x[2]$$

$$= -a (-a y[0] + b x[1]) + b x[2]$$

$$= a^2 y[0] - a b x[1] + b x[2]$$

9.15.03 Ch2 - System Definition

$$n=3 \quad y[3] = -ay[2] + bx[3]$$

$$= -a(a^2y[0] - abx[1] + bx[2]) + bx[3]$$

$$= -a^3y[0] + a^2bx[1] - abx[2] + bx[3]$$

$$\begin{matrix} \uparrow & \uparrow & \uparrow & \uparrow \\ (-a)^n & (-a)^{n-1}b & (-a)^{n-2}b & (-a)^{n-3}b \end{matrix}$$

$$\therefore y[n] = (-a)^n y[0] + \sum_{i=1}^n (-a)^{n-i} b x[i]$$

2.19 / (b) closed-form sol'n for $y[n]$ w/ $x[n] = u[n]$, $y[0] = 0$

$$(i) \quad y[n+1] + 1.5y[n] = x[n]$$

$$n=0 \quad y[1] = -1.5y[0] + x[1] \\ = 1$$

$$n=1 \quad y[2] = -1.5y[1] + x[1] \\ = -1.5(1) + 1$$

$$n=2 \quad y[3] = -1.5y[2] + x[2] \\ = -1.5(-1.5y[1] + 1) + 1 \\ = (-1.5)^2 y[1] - 1.5 + 1$$

$$n=3 \quad y[4] = -1.5[(-1.5)^2 y[1] - 1.5 + 1] + 1 \\ = (-1.5)^3 y[1] + (-1.5)^2 + (-1.5) + 1 \\ = (-1.5)^{n-1} + (-1.5)^{n-2} + (-1.5)^{n-3} + (-1.5)^{n-4} \\ = \sum_{i=1}^n (-1.5)^{n-i}$$

9.15.03 Ch 2 - System Definition

2.19/

$$y[n] = \sum_{i=1}^n (-1.5)^{n-i}$$

Note. $\sum_{i=1}^N a^i = \frac{a - a^{N+1}}{1-a}$

Eqn. $\sum_{i=0}^N a^i = \frac{1 - a^{N+1}}{1-a}$

$$y[n] = (-1.5)^n \cdot \sum_{i=1}^n (-1.5)^{-i}$$

$$= (-1.5)^n \cdot \sum_{i=1}^n \left(\frac{-1}{1.5} \right)^i$$

$$= (-1.5)^n \cdot \frac{(-1/1.5) - (-1/1.5)^{n+1}}{1 - (-1/1.5)}$$

$$= \frac{(-1.5)^{n-1} - (-1.5)^n \cdot (-1/1.5)^{n+1}}{(2.5/1.5)}$$

$$= \frac{1}{2.5} \cdot (1.5) \cdot (-1.5)^{n-1} - \frac{1}{2.5} \cdot (1.5) \cdot (-1.5)^n \cdot (-1.5)^{-(n+1)}$$

$$= \frac{0.4 \cdot (1.5) \cdot (-1.5)^n - 0.4 \cdot (1.5) \cdot (-1.5)^{-1}}{-1.5}$$

$$= -0.4 (-1.5)^n + 0.4 \quad n \geq 0$$

(c) closed-form $y[n]$ w/ $x[n] = u[n]$, $y[0] = 2$

$$n=0 \quad y[1] = -1.5 y[0] + x[0]$$

$$n=1 \quad y[2] = -1.5 y[1] + x[1]$$

$$= -1.5 [-1.5 y[0] + x[0]] + x[1]$$

$$= (-1.5)^2 y[0] - 1.5 x[0] + x[1]$$

9.15.03 Ch 2 System Definition

2.19/ $n=2$ $y[3] = -1.5y[2] + x[2]$

$$= (-1.5)^3 y[0] + (-1.5)^2 x[0] + (-1.5)^1 x[1] + (-1.5)^0 x[2]$$

$$\therefore y[n] = (-1.5)^n y[0] + \sum_{i=1}^n (-1.5)^{n-i} x[i-1] \quad i \geq 1$$

$$= 2 \cdot (-1.5)^n + \sum_{i=1}^n (-1.5)^{n-i}$$

~~~~~

can use previous answer.

## 9.15.03 Ch 3 Convolution Representation.

### DISCRETE TIME LTI SYSTEMS

Note: - Assume  $y[n]$  is output response from  $x[n]$  (input)  
w/ no initial energy prior to application of  $x[n]$  !

### UNIT-PULSE RESPONSE

$$\text{if input } x[n] = \delta[n] = \begin{cases} 1 & n=0 \\ 0 & n \neq 0 \end{cases}$$

↓ then

$$\text{output } y[n] = h[n] \sim \text{unit-pulse response}$$

Given system response to single pulse, if system is causal LTI,  
then output response  $y[n]$  can be computed for any  
arbitrary input  $x[n]$

Assume input  $x[n] = 0$  for  $n = -1, -2, \dots$

$$\text{for any shift in time } i, \delta[n-i] = \begin{cases} 1 & n=i \\ 0 & n \neq i \end{cases}$$

$$\begin{aligned} \therefore x[n] &= x[0]\delta[n] + x[1]\delta[n-1] + x[2]\delta[n-2] + \dots \\ &= \sum_{i=0}^{\infty} x[i]\delta[n-i] \quad n=0,1,2,\dots \end{aligned}$$

# 9.15.03 Ch 3 Convolution Representation

Since system is LTI, system <sup>output</sup> response to input  $x[i] \delta[n-i]$

$$\Downarrow$$

$$y_i[n] = x[i] h[n-i]$$

complete solution is thus

$$y[n] = \sum_{i=0}^{\infty} y_i[n] = \sum_{i=0}^{\infty} x[i] h[n-i] \quad n \geq 0 \quad (\text{CAUSAL})$$

CONVOLUTION of  $x[n] \neq h[n]$

$$\sum_{i=0}^{\infty} x[i] h[n-i] = \underset{\substack{\uparrow \\ \text{input}}}{x[n]} * \underset{\substack{\uparrow \\ \text{unit-pulse response}}}{h[n]} = \underset{\substack{\uparrow \\ \text{output}}}{y[n]} \quad n \geq 0$$

In essence, system is completely determined by  $h[n]$

$\therefore$  if  $h[n]$  is known, output response  $y[n]$  from any arbitrary  $x[n]$  can be determined via

$$y[n] = x[n] * h[n]$$

9.17.03

## DISCRETE-TIME CONVOLUTION

in general  $x[n] * v[n] = \sum_{i=-\infty}^{\infty} x[i] v[n-i] \quad (\text{CONVOLUTION SUM})$

$$\text{if } x[n] = 0 \text{ for } n < 0 \neq v[n] = 0 \text{ for } n < 0$$

$$\Downarrow \qquad \qquad \qquad \Downarrow$$

$$x[i] = 0 \quad i < 0 \qquad v[n-i] = 0 \quad n-i < 0 \quad (n < i)$$

$$\therefore x[n] * v[n] = \begin{cases} 0 & n = -1, -2, \dots \\ \sum_{i=0}^n x[i] v[n-i] & n = 0, 1, 2, \dots \end{cases}$$

## 9.17.03 Ch3 Convolution Representation

Convolution process: convolving  $x[n]$  &  $v[n]$

1/ change  $n \rightarrow i$   $\therefore x[n] \rightarrow x[i]$   
 $v[n] \rightarrow v[i]$

2/ create  $v[n-i]$  by

a/ fold  $v[i]$  about  $i=0$  axis  $\rightarrow v[-i]$   
b/ time shift  $v[-i]$  by  $n \rightarrow v[n-i]$

3/ once  $x[i]$  &  $v[n-i]$  generated, sum elements

$$\sum_{i=-\infty}^{\infty} x[i] v[n-i]$$

Emphasize value of text examples 3.2 & 3.3.

graphical  $\uparrow$   
analytical  $\uparrow$

PROPERTIES OF CONVOLUTION OPERATION  $x[n] * v[n]$

Associativity -  $x[n] * (v[n] * w[n]) = (x[n] * v[n]) * w[n]$

Commutativity -  $x[n] * v[n] = v[n] * x[n]$

$\Downarrow$

$$\sum_{i=-\infty}^{\infty} x[i] v[n-i] = \sum_{i=-\infty}^{\infty} v[i] x[n-i]$$

Distributivity w/ addition -

$$x[n] * (v[n] + w[n]) = x[n] * v[n] + x[n] * w[n]$$

Convolution w/ unit pulse -  $x[n] * \delta[n] = x[n]$

Convolution w/ shifted unit pulse -  $x[n] * \delta[n-q] = x[n-q]$

9-17-03 Ch3 Convolution Representation

Causal LTI System

$$y[n] = x[n] * h[n] = \sum_{i=-\infty}^{\infty} x[i] h[n-i] \quad n \geq 0$$

$\uparrow$   
 $x[n] = 0, n < 0$

Since  $h[n] = 0, n < 0$  (causality)  $\rightarrow h[n-i] = 0, i > n$

$$\begin{aligned} \therefore y[n] &= \sum_{i=0}^n x[i] h[n-i] \quad n \geq 0 \\ &= \sum_{i=0}^n h[i] x[n-i] \quad n \geq 0 \end{aligned}$$

since  $x[n] * h[n] = h[n] * x[n]$

If system is non-causal  $\rightarrow h[n] \neq 0$  for  $n < 0$

$$y[n] = \sum_{i=-\infty}^{\infty} x[i] h[n-i]$$

if  $x[n] \neq 0, n < 0$  and noncausal system

$$y[n] = \sum_{i=-\infty}^{\infty} x[i] h[n-i]$$

9-22-03

CONTINUOUS-TIME LTI SYSTEMS.

Note: Assume  $y(t)$  is response from  $x(t)$  (input)  
w/ no initial energy in system prior to application of  $x(t)$

IMPULSE RESPONSE if  $x(t) = \delta(t) \rightarrow y(t) = h(t)$

remember

$$\delta(t) = 0 \quad t \neq 0$$

$$\int_{-\epsilon}^{\epsilon} \delta(t) dt = 1 \quad \text{for any } \epsilon > 0.$$

$\uparrow$   
impulse response

### 9.22.03 Ch3 Convolution Representation

As in discrete-time case,  $x(t) = \delta(t) \rightarrow h(t)$

$$x(t) = \delta(t-\lambda) \rightarrow h(t-\lambda)$$

if  $x(t)$  is arbitrary input w/  $x(t) = 0$   $t < 0$

then

$$x(t) = \int_{0^-}^{\infty} x(\lambda) \delta(t-\lambda) d\lambda \quad t \geq 0.$$

given input  $x(\lambda) \delta(t-\lambda)$  and  $\delta(t-\lambda) \rightarrow h(t-\lambda)$

↓  
output  $y_\lambda(t) = x(\lambda) h(t-\lambda)$

integrating over all  $\lambda$  gives

$$y(t) = \int_{0^-}^{\infty} x(\lambda) h(t-\lambda) d\lambda \quad t \geq 0.$$

In general,  $x(\lambda) h(t-\lambda)$  does not contain impulse @  $\lambda = 0$ .  
As such,

$$\begin{aligned} y(t) &= \int_0^{\infty} x(\lambda) h(t-\lambda) d\lambda \quad t \geq 0 \\ &= x(t) * h(t) \quad t \geq 0 \end{aligned}$$

As in discrete-time case, system is completely determined by  $h(t)$  in that if  $h(t)$  is known, output response to any arbitrary input can be computed.

CONTINUOUS-TIME CONVOLUTION.

$$x(t) * v(t) = \int_{-\infty}^{\infty} x(\lambda) v(t-\lambda) d\lambda \quad (\text{CONVOLUTION INTEGRAL})$$

$$\left. \begin{array}{l} \text{if } x(t) = 0 \quad t < 0 \\ \text{if } v(t) = 0 \quad t < 0 \end{array} \right\} \rightarrow x(t) * v(t) = \int_0^t x(\lambda) h(t-\lambda) d\lambda \quad t \geq 0$$

9.22.03 Ch 3 - Convolution Representation.

Continuous Time Convolution Process.

1/ Graph  $x(\lambda)$  &  $v(-\lambda)$  as fn of  $\lambda$

2/ Define interval  $[0, a]$

graph  $v(t-\lambda)$   
&  $x(\lambda)v(t-\lambda)$

↑ largest value of  $a$   
for which  $x(\lambda)v(t-\lambda)$   
has same analytical form for all  $t \in [0, a]$

3/ w/  $0 \leq t \leq a \rightarrow \int_{\lambda=0}^t x(\lambda)v(t-\lambda)d\lambda$   
 $= x(t) * v(t)$  over  $t \in [0, a]$

4/ Define interval  $[a, b]$

graph  $v(t-\lambda)$   
&  $x(\lambda)v(t-\lambda)$

↑ largest value of  $b$   
for which  $x(\lambda)v(t-\lambda)$   
has same analytical form for all  $t \in [a, b]$

5/ w/  $a \leq t \leq b \rightarrow \int_{\lambda=0}^t x(\lambda)v(t-\lambda)d\lambda$   
 $= x(t) * v(t)$  over  $t \in [a, b]$

6/ Repeat steps 4 & 5 until  $x(t) * v(t)$  is computed  
for all  $t > 0$ .

Encourage students to review Examples <sup>2.15 2.16</sup> 3.7 & 3.8 in text.



# 9.22.03 Ch 3 - Convolution Representation

## PROPERTIES OF CONVOLUTION

ASSOCIATIVITY  $[x(t) * v(t)] * w(t) = x(t) * [v(t) * w(t)]$

COMMUTATIVITY  $x(t) * v(t) = v(t) * x(t)$

$$\therefore \int_{-\infty}^{\infty} x(\lambda) v(t-\lambda) d\lambda = \int_{-\infty}^{\infty} v(\lambda) x(t-\lambda) d\lambda$$

DISTRIBUTIVITY w/ ADDITION  $x(t) * [v(t) + w(t)] = x(t) * v(t) + x(t) * w(t)$

DERIVATIVE PROPERTY  $\frac{d}{dt} [x(t) * v(t)] = \dot{x}(t) * v(t) = \dot{v}(t) * x(t) = \frac{d}{dt} [v(t) * x(t)]$

## CONVOLUTION w/ UNIT IMPULSE

$$\begin{aligned} x(t) * \delta(t) &= \delta(t) * x(t) = \int_{-\infty}^{\infty} \delta(\lambda) x(t-\lambda) d\lambda \\ &= \int_{-\infty}^{\infty} \delta(\lambda) x(t) d\lambda \\ &= x(t) \int_{-\infty}^{\infty} \delta(\lambda) d\lambda \\ &= x(t) \end{aligned}$$

## CONVOLUTION w/ SHIFTED UNIT IMPULSE

if  $\delta_c(t) = \delta(t-c) \rightarrow x(t) * \delta(t-c) = x(t-c)$

## Causal LTI Systems

$$\uparrow \quad y(t) = x(t) * h(t) = \int_0^t x(\lambda) h(t-\lambda) d\lambda \quad t \geq 0$$

$h(t) = 0 \quad t < 0$

$\uparrow \quad x(t) = 0, \quad t < 0$

by causality  $\rightarrow$  upper limit on  $\int^t$  is  $t$ .

9.22.03 Ch 3 - Convolution Representation

$$\text{also, } y(t) = h(t) * x(t) = \int_0^t h(\lambda) x(t-\lambda) d\lambda \quad t \geq 0.$$

Going back to  $y(t) = x(t) * h(t) = \int_0^t x(\lambda) h(t-\lambda) d\lambda \quad t \geq 0$

if system is non-causal  $\rightarrow h(t) \neq 0$  for  $t < 0$

$\Downarrow$

$$y(t) = \int_0^{\infty} x(\lambda) h(t-\lambda) d\lambda$$

if  $x(t) \neq 0$  for  $t < 0$  and system is noncausal,

$\Downarrow$

$$y(t) = \int_{-\infty}^{\infty} x(\lambda) h(t-\lambda) d\lambda$$

9.24.03 Ch 4 - Fourier Series / Fourier Transform

$x(t)$  ~ arbitrary signal

$\uparrow$   
usually expressed/generated in time domain

signals w/ sharp (temporal) transitions are well-characterized in time domain } impulse, pulse, pulse trains.

some signals have features that are better characterized in other domains

- $\rightarrow$  frequency
- $\rightarrow$  wavelet
- $\rightarrow$  transform domain

Fourier analysis  $\rightarrow$  Fourier domain = Frequency domain

9.24.03

# Ch 4 Fourier Series / Fourier Transform

## Frequency Content

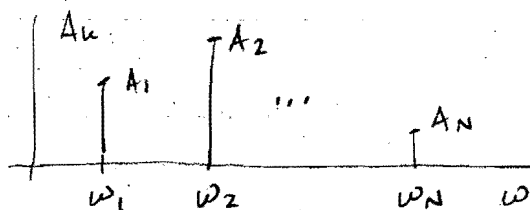
- generated by decomposing  $x(t)$  into constituent sinusoids.

In general, suppose 
$$x(t) = \sum_{k=1}^N A_k \cos(\omega_k t + \theta_k) \quad -\infty < t < \infty$$

$\left\{ \begin{array}{l} \{A_1, A_2, \dots, A_N\} \text{ are amplitudes (nonnegative)} \\ \{\omega_1, \omega_2, \dots, \omega_N\} \text{ are frequencies (rad/sec)} \\ \{\theta_1, \theta_2, \dots, \theta_N\} \text{ are phases (radians)} \end{array} \right.$   
 together, completely describe  $x(t)$

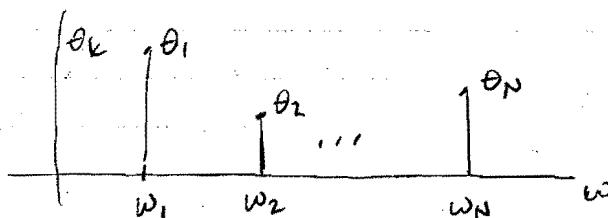
- Plotting  $A_k$  vs.  $\omega_k$

AMPLITUDE SPECTRUM  
(LINE SPECTRUM)



- Plotting  $\theta_k$  vs.  $\omega_k$

PHASE SPECTRUM  
(LINE SPECTRUM)



Euler's Formula

$$A_k e^{j(\omega_k t + \theta_k)} = A_k \cos(\omega_k t + \theta_k) + j A_k \sin(\omega_k t + \theta_k)$$

$$\therefore A_k \cos(\omega_k t + \theta_k) = \text{Re} \{ A_k e^{j(\omega_k t + \theta_k)} \}$$

$\Downarrow$

$$x(t) = \sum_{k=1}^N \text{Re} \{ A_k e^{j(\omega_k t + \theta_k)} \}$$

9.24.03 Ch 4 - Fourier Series / Fourier Transform

Furthermore,

$$\operatorname{Re}\{A_k e^{j(\omega_k t + \theta_k)}\} = \frac{A_k}{2} e^{j(\omega_k t + \theta_k)} + \frac{A_k}{2} e^{-j(\omega_k t + \theta_k)}$$

$$\therefore x(t) = \sum_{k=1}^N \left[ \frac{A_k}{2} e^{j(\omega_k t + \theta_k)} + \frac{A_k}{2} e^{-j(\omega_k t + \theta_k)} \right]$$

if we let  $c_k = \frac{A_k}{2} e^{j\theta_k}$  &  $c_{-k} = \frac{A_k}{2} e^{-j\theta_k}$

then

$$x(t) = \sum_{k=1}^N \left[ c_k e^{j\omega_k t} + c_{-k} e^{-j\omega_k t} \right]$$

$$= \sum_{k=1}^N c_k e^{j\omega_k t} + \sum_{k=1}^N c_{-k} e^{j(-\omega_k) t}$$

↑  
"negative" frequency  
- mathematical abstraction  
- no physical meaning

$$x(t) = \sum_{\substack{k=-N \\ k \neq 0}}^N c_k e^{j\omega_k t}$$

$$c_k = \frac{A_k}{2} [\cos \theta_k + j \sin \theta_k] \quad k=1, 2, \dots, N$$

$$c_{-k} = \frac{A_k}{2} [\cos \theta_k - j \sin \theta_k] \quad k=1, 2, \dots, N$$

↑  
Note:  $c_k$  &  $c_{-k}$  are real iff  $\sin \theta_k = 0$

↓  
 $\theta_k = n\pi$   
 $n$  is integer

Also,  $|c_k| = \frac{A_k}{2} = |c_{-k}| \quad k=1, 2, \dots$

↑  
magnitude → Amplitude spectrum is even fn of  $\omega$

$$\angle c_k = -\angle c_{-k} \quad k=1, 2, \dots$$

↑  
phase → phase spectrum is odd fn of  $\omega$ .

9.24.03 Ch 4 Fourier Series / Fourier Transform.

In general,  $x(t) = \sum_{k=1}^N A_k \cos(\omega_k t + \theta_k) \quad -\infty < t < \infty$

↑  
limited # of signals can be represented by this expression

if  $N \rightarrow \infty$ , then

$$x(t) = \sum_{k=1}^{\infty} A_k \cos(\omega_k t + \theta_k) \quad -\infty < t < \infty$$

↑  
set of signals includes periodic signals.

9.29.03

FOURIER SERIES REPRESENTATION OF PERIODIC SIGNALS.

Periodic signals  $x(t+T) = x(t) \quad \forall t \quad -\infty < t < \infty$

↑  
fundamental period  $T$   
[smallest  $\Delta t$  for which]  
 $x(t+\Delta t) = x(t)$

if  $x(t)$  is PERIODIC w/ period  $T$ ,  $x(t)$  can be expressed as sum of complex exponentials

i.e.,

$$x(t) = \sum_{k=-\infty}^{\infty} c_k e^{jk\omega_0 t} \quad -\infty < t < \infty$$

Fourier series of  
periodic signal  $x(t)$

$$\omega_0 = \frac{2\pi}{T} \text{ rad/sec}$$

fundamental frequency

Determining  $c_k \rightarrow$

$$c_k = \frac{1}{T} \int_{-T/2}^{T/2} x(t) e^{-jk\omega_0 t} dt \quad k = 0, \pm 1, \pm 2, \dots$$

integral valid over

$$\text{any full period s.t. } c_k = \frac{1}{T} \int_0^T x(t) e^{-jk\omega_0 t} dt \quad k = 0, \pm 1, \pm 2, \dots$$

$$\int x e^{ax} dx = \frac{e^{ax}}{a^2} (ax - 1)$$

## 9.29 03 Ch4 Fourier Series/Fourier Transform

For  $k=0 \rightarrow$  dc component  $x(t)e^{j0\omega t} = x(t)$

$$c_0 = \frac{1}{T} \int_{-T/2}^{T/2} x(t) dt$$

In general, a periodic signal  $x(t)$  has a Fourier Series if it satisfies DIRICHLET CONDITIONS

1/  $x(t)$  is absolutely integrable over any period

$$\int_a^{a+T} |x(t)| dt < \infty \text{ for any } a$$

2/  $x(t)$  finite number of maxima/minima over any period

3/  $x(t)$  finite number of discontinuities over any period.

Gibbs Phenomenon - Recitation: MATLAB p. 161

Parseval's Theorem

$x(t) \sim$  periodic w/ period  $T$

average power  $\rightarrow P = \frac{1}{T} \int_{-T/2}^{T/2} x^2(t) dt$  integrate over time

$$= \sum_{k=-\infty}^{\infty} |c_k|^2$$

sum over line spectra.

9.29.03 Ch4 Fourier Series / Fourier Transform

## FOURIER TRANSFORM

periodic signals  $\rightarrow$  Fourier Series

What about nonperiodic (aperiodic) signals?

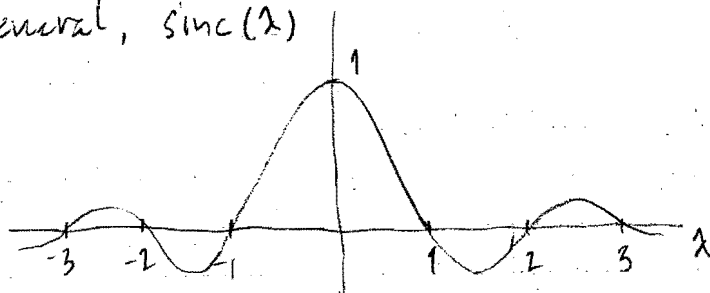


Fourier Transform (continuous  $\omega$ )

Note: book goes through derivation from  $k\omega_0 \rightarrow \omega$   
(as  $T \rightarrow \infty$ )  
 $\uparrow$   
in so doing, uses  $\text{sinc}(\cdot)$  fn.

$$\text{sinc } \lambda = \frac{\sin(\pi \lambda)}{\pi \lambda}$$

in general,  $\text{sinc}(\lambda)$



zero crossings @  $\lambda = \pm 1, \pm 2, \dots$

$\text{sinc}(0) = 1$  w/ subsequent sidelobes of decreasing magnitude

10.01.03

## FOURIER TRANSFORM

$$X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt \quad -\infty < \omega < \infty$$

$\uparrow$   $\omega$  is continuous frequency

cf. Fourier Series w/  $c_k = \frac{1}{T} \int_{-T/2}^{T/2} x(t) e^{-jk\omega_0 t} dt \quad k = 0, \pm 1, \pm 2, \dots$

$\uparrow$   
harmonics of fundamental freq.  
( $k\omega_0$ )  
( $\omega_0 = \frac{2\pi}{T}$ )



INVERSE Fourier Transform  $X(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(\omega) e^{j\omega t} d\omega$

$$\therefore X(t) \xrightleftharpoons[\text{IFT}]{\text{FT}} X(\omega)$$

Fourier Transform exists if  $X(t)$  is absolutely integrable

$$\int_{-\infty}^{\infty} |X(t)| dt < \infty$$

"well-behaved" - finite # of discontinuities,  
maxima, minima w/in any finite  $\Delta t$

All actual signals are well-behaved and, thus, absolutely integrable.

$$X(\omega) = \int_{-\infty}^{\infty} X(t) e^{-j\omega t} dt$$

Complex quantity (even though  $\omega$  is REAL)

$$\begin{aligned} X(\omega) &= \int_{-\infty}^{\infty} X(t) \cos(\omega t) dt - j \int_{-\infty}^{\infty} X(t) \sin(\omega t) dt \\ &= R(\omega) + j I(\omega) \end{aligned}$$

$$\text{where } R(\omega) = \int_{-\infty}^{\infty} X(t) \cos(\omega t) dt$$

$$\text{and } I(\omega) = - \int_{-\infty}^{\infty} X(t) \sin(\omega t) dt$$

Polar form  $\rightarrow X(\omega) = |X(\omega)| e^{j\angle X(\omega)}$

$$\text{where } |X(\omega)| = (R^2(\omega) + I^2(\omega))^{1/2}$$

$$\angle X(\omega) = \arctan(I(\omega)/R(\omega))$$

10-01-03 Ch 4 Fourier Series / Fourier Transform

Note:

If  $x(t)$  is REAL valued,

↓

$$X(-\omega) = \overline{X(\omega)} = |X(\omega)| e^{-j\angle X(\omega)}$$

$$\therefore |X(-\omega)| = |X(\omega)|$$

$$\angle X(-\omega) = -\angle X(\omega)$$

SIGNALS w/ SYMMETRY - EVEN OR ODD.

↓

$$x(t) = x(-t)$$

↓

$$x(-t) = -x(t)$$

↓

$$R(\omega) = 2 \int_0^{\infty} x(t) \cos(\omega t) dt$$

$$R(\omega) = 0$$

$$I(\omega) = 0$$

$$I(\omega) = -2 \int_0^{\infty} x(t) \sin(\omega t) dt$$

↓

If  $x(t)$  is EVEN,

↓

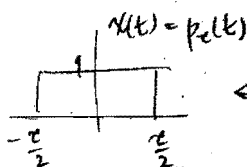
If  $x(t)$  is ODD,

$$X(\omega) = 2 \int_0^{\infty} x(t) \cos(\omega t) dt$$

$$X(\omega) = -j 2 \int_0^{\infty} x(t) \sin(\omega t) dt$$

EXAMPLE

rectangular pulse -  $x(t) = p_{\tau}(t) = \begin{cases} 1 & -\frac{\tau}{2} \leq t < \frac{\tau}{2} \\ 0 & \text{o.w.} \end{cases}$



← even fn. of  $t \therefore X(\omega) = 2 \int_{-\tau/2}^{\tau/2} 1 \cos(\omega t) dt$

$$= \frac{2}{\omega} \sin(\omega t) \Big|_{-\tau/2}^{\tau/2}$$

$$= \frac{2}{\omega} \sin\left(\frac{\omega \tau}{2}\right)$$

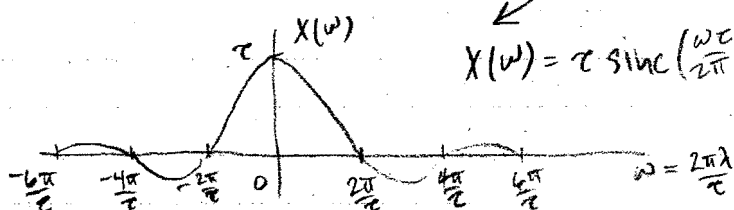
$$= \tau \cdot \frac{\sin\left(\frac{\omega \tau}{2}\right)}{\left(\frac{\omega \tau}{2}\right)}$$

$$= \tau \cdot \text{sinc}\left(\frac{\omega \tau}{2\pi}\right)$$

$$\left. \begin{array}{l} \\ \end{array} \right\} \pi \lambda = \frac{\omega \tau}{2}$$

recall  $\text{sinc}(\lambda) = \frac{\sin(\pi \lambda)}{\pi \lambda}$

$$X(\omega) = \tau \text{sinc}\left(\frac{\omega \tau}{2\pi}\right)$$



## BANDLIMITED SIGNALS.

$x(t)$  is BANDLIMITED if  $X(\omega) = 0 \quad \omega > B$

↑  
positive integer  
(bandwidth)

Notes:

bandlimited signals can NOT be time limited.

$\therefore$  finite  $B \rightarrow$  infinite time span (duration)!

likewise,

finite time duration  $\rightarrow$  infinite bandwidth!  
( $B$ )

## PROPERTIES OF FOURIER TRANSFORM.

## LINEARITY

$$aX(t) + bV(t) \leftrightarrow aX(\omega) + bV(\omega)$$

(result of linearity of integration)

## LEFT/RIGHT TIME-SHIFT

$$x(t-c) \leftrightarrow X(\omega) e^{-j\omega c}$$

## TIME SCALING

$$x(at) \leftrightarrow \frac{1}{a} X\left(\frac{\omega}{a}\right) \quad a > 0$$

Note:  $0 < a < 1$  time expansion  $\rightarrow$  frequency compression

$a > 1$  time compression  $\rightarrow$  frequency expansion

time-limited vs. band-limited.

10.01.03 Ch4 Fourier Series / Fourier Transform.

TIME REVERSAL

$$x(-t) \leftrightarrow X(-\omega)$$

Note: if  $x(t)$  is real valued, then  $X(-\omega) = \overline{X(\omega)}$

$$\therefore x(-t) \leftrightarrow \overline{X(\omega)} \quad x(t) \text{ is REAL.}$$

MULTIPLICATION BY POWER OF  $t$

$$t^n x(t) \leftrightarrow (j)^n \frac{d^n}{d\omega^n} X(\omega)$$

MULTIPLICATION BY A COMPLEX EXPONENTIAL

$$x(t) e^{j\omega_0 t} \leftrightarrow X(\omega - \omega_0) \quad \text{frequency modulation}$$

↓

$$x(t) \cos(\omega_0 t) \leftrightarrow \frac{1}{2} [X(\omega + \omega_0) + X(\omega - \omega_0)]$$

$$x(t) \sin(\omega_0 t) \leftrightarrow \frac{j}{2} [X(\omega + \omega_0) - X(\omega - \omega_0)]$$

TIME DOMAIN DIFFERENTIATION / INTEGRATION

$$\frac{d^n}{dt^n} x(t) \leftrightarrow (j\omega)^n X(\omega)$$

$$\int_{-\infty}^t x(\lambda) d\lambda \leftrightarrow \frac{1}{j\omega} X(\omega)$$

TIME DOMAIN CONVOLUTION / MULTIPLICATION

$$x(t) * v(t) \leftrightarrow X(\omega) V(\omega)$$

$$x(t) v(t) \leftrightarrow \frac{1}{2\pi} [X(\omega) * V(\omega)]$$

DUALITY

$$X(t) \leftrightarrow 2\pi X(-\omega)$$

↑  
if we know FT in one direction, can apply it to similar signals

# 10-06-03 Ch 4 Fourier Series / Fourier Transform

## PARSEVAL'S THEOREM

$$\int_{-\infty}^{\infty} x(t) v(t) dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} \overline{X(\omega)} V(\omega) d\omega$$

## GENERALIZED FOURIER TRANSFORM

Some common fns don't have FT in ordinary sense  $\begin{cases} u(t) \\ \cos(\omega_0 t) \\ \sin(\omega_0 t) \end{cases}$

$\uparrow$   
 $x(t) = 1$  is not absolutely integrable  
 $\forall t$

$\Downarrow$   
 Generalized  
 Fourier Transform.

By conventional approach,  $\delta(t) \longleftrightarrow 1 \quad -\infty < \omega < \infty$

Using DUALITY property  $x(t) \longleftrightarrow 2\pi x(-\omega)$

if  $x(t) = \delta(t) \longrightarrow X(\omega) = 1 \quad -\infty < \omega < \infty$

then by DUALITY  $x(t) = 1 \quad -\infty < t < \infty \longrightarrow 2\pi X(-\omega) = 2\pi \delta(\omega)$

$\therefore$   
 $1 \longleftrightarrow 2\pi \delta(\omega)$   
 constant in time  $\longleftrightarrow$  impulse in frequency.

other pairs.

$$\cos(\omega_0 t) \longleftrightarrow \pi [\delta(\omega + \omega_0) + \delta(\omega - \omega_0)]$$

$$\sin(\omega_0 t) \longleftrightarrow j\pi [\delta(\omega + \omega_0) - \delta(\omega - \omega_0)]$$

$$e^{j\omega_0 t} \longleftrightarrow 2\pi \delta(\omega - \omega_0)$$

$$u(t) \longleftrightarrow \frac{1}{j\omega} + \pi \delta(\omega)$$

LTI system

$$x_c(t) = A e^{j(\omega_0 t + \theta)} \quad -\infty < t < \infty$$

↓

$$y_c(t) = x_c(t) * h(t)$$

$$= \int_{-\infty}^{\infty} h(\lambda) x_c(t-\lambda) d\lambda$$

$$= \int_{-\infty}^{\infty} h(\lambda) A e^{j(\omega_0(t-\lambda) + \theta)} d\lambda$$

$$= \int_{-\infty}^{\infty} h(\lambda) e^{-j\omega_0 \lambda} d\lambda [A e^{j(\omega_0 t + \theta)}]$$

$$= x_c(t) \int_{-\infty}^{\infty} h(\lambda) e^{-j\omega_0 \lambda} d\lambda$$

$$= x_c(t) H(\omega_0)$$

↑  
complex fn. (magnitude  
phase)  
↑  
eigenfunction

10.06.03 Ch 5 Frequency Domain Analysis.

LTI Continuous-time system

$$y(t) = x(t) * h(t) = \int_{-\infty}^{\infty} x(\lambda) h(t-\lambda) d\lambda = \int_{-\infty}^{\infty} h(\lambda) x(t-\lambda) d\lambda$$

Note: throughout Ch 5, assumed that  $h(t)$  is absolutely integrable.

$$\Downarrow$$

$$h(t) \rightarrow H(\omega) \text{ exists.}$$

$\therefore$  Assuming  $H(\omega)$  exists, given

$$H(\omega) = \int_{-\infty}^{\infty} h(t) e^{-j\omega t} dt$$

$$x(t) = A \cos(\omega_0 t + \theta) \quad -\infty < t < \infty \quad = |H(\omega)| e^{j\angle H(\omega)}$$

$$\downarrow$$

$$\boxed{h(t) \leftrightarrow H(\omega)} \quad \text{LTI System - see opposite page.}$$

$$\downarrow$$

$$y(t) = A |H(\omega_0)| \cos(\omega_0 t + \theta + \angle H(\omega_0)) \quad -\infty < t < \infty$$

$$H(\omega) \text{ frequency response } \left\{ \begin{array}{l} |H(\omega)| \text{ magnitude fn} \\ \angle H(\omega) \text{ phase fn.} \end{array} \right.$$

$$\downarrow$$

$$H(\omega)|_{\omega=\omega_0} = H(\omega_0) \sim \text{frequency response at particular frequency}$$

RESPONSE TO PERIODIC INPUTS

$$\text{periodic} \rightarrow c_k = f(k\omega_0) \rightarrow H(k\omega_0)$$

$$\text{Suppose } x(t) = \sum_{k=-\infty}^{\infty} c_k e^{jk\omega_0 t} \quad -\infty < t < \infty$$

$$\downarrow$$

$$\boxed{h(t) \leftrightarrow H(\omega)}$$

$$\downarrow$$

$$y(t) = \sum_{k=-\infty}^{\infty} H(k\omega_0) c_k e^{jk\omega_0 t} \quad -\infty < t < \infty$$

$\therefore$  if  $x(t+T) = x(t)$  } response to periodic input w/ fund period T  
 then  $y(t+T) = y(t)$  } is periodic w/ fund period T

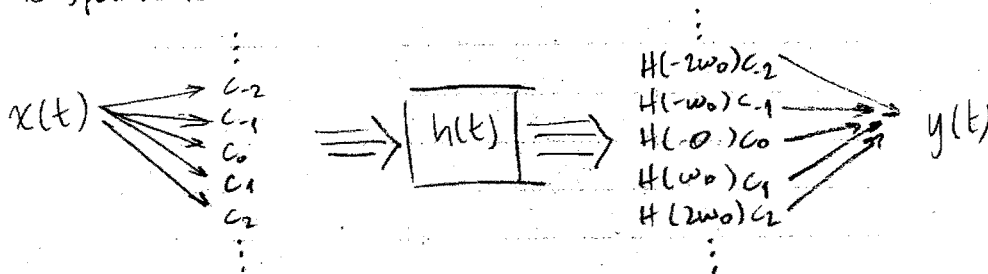
10.06.03 Ch 5 Frequency Domain Analysis.

$$x(t) = \sum_{k=-\infty}^{\infty} c_k e^{jk\omega_0 t} \rightarrow y(t) = \sum_{k=-\infty}^{\infty} H(k\omega_0) c_k e^{jk\omega_0 t}$$

$$= \sum_{k=-\infty}^{\infty} |H(k\omega_0)| |c_k| e^{j(k\omega_0 t + \angle c_k + \angle H(k\omega_0))}$$

$\uparrow$  magnitude scaled (gain/attenuation)       $\uparrow$  phase shifted (linear delay or distortion) group delay

$\therefore$  Response to PERIODIC INPUT is as if

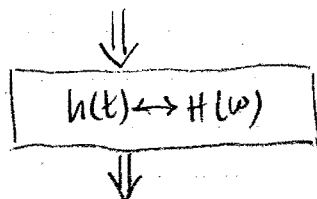


Remember  $x(t) * h(t) \rightarrow X(\omega) H(\omega)$

$\uparrow$   
(line spectra for PERIODIC signal)

RESPONSE TO APERIODIC INPUTS.

$$x(t) \rightarrow X(\omega)$$



$$|Y(\omega)| = |X(\omega)| |H(\omega)|$$

$$\angle Y(\omega) = \angle X(\omega) + \angle H(\omega)$$

$$Y(\omega) = X(\omega) H(\omega)$$

$$y(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(\omega) H(\omega) e^{j\omega t} d\omega$$

$\uparrow$  note error in text p.216

$\uparrow$  assumes no initial energy in system prior to application of  $x(t)$ .



$$H(\omega) = p_{2B}(\omega) e^{-j\omega t_d} \quad -\infty < \omega < \infty$$

we know  $\frac{\tau}{2\pi} \text{sinc} \frac{\tau t}{2\pi} \leftrightarrow p_{\tau}(\omega)$

$\Downarrow$

$$p_{2B}(\omega) \rightarrow \frac{2B}{2\pi} \text{sinc} \frac{2Bt}{2\pi} = \frac{B}{\pi} \text{sinc} \left( \frac{B}{\pi} t \right)$$

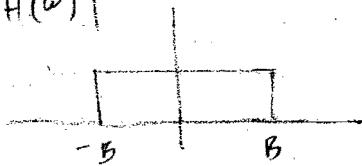
$\downarrow$

$$p_{2B}(\omega) e^{-j\omega t_d} \rightarrow \frac{B}{\pi} \text{sinc} \left( \frac{B}{\pi} (t - t_d) \right)$$

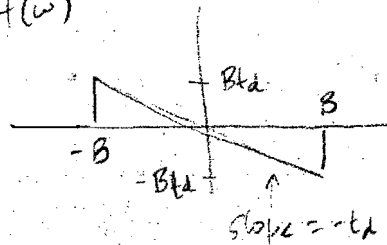
$$\therefore H(\omega) = p_{2B}(\omega) e^{-j\omega t_d} \rightarrow h(t) = \frac{B}{\pi} \text{sinc} \left( \frac{B}{\pi} (t - t_d) \right)$$

$\downarrow$

$|H(\omega)|$



$\angle H(\omega)$

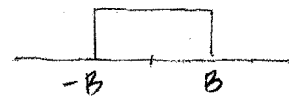


# 10-08-03 Ch 5 Frequency Domain Analysis

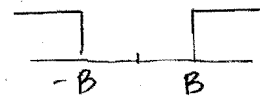
## ANALYSIS OF IDEAL FILTERS.

MAGNITUDE FUNCTIONS:

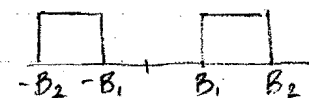
Ideal Lowpass  $|H(\omega)| = \begin{cases} 1 & -B \leq \omega \leq B \\ 0 & |\omega| > B \end{cases}$



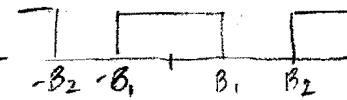
Ideal Highpass  $|H(\omega)| = \begin{cases} 0 & -B < \omega < B \\ 1 & |\omega| \geq B \end{cases}$



Ideal Bandpass  $|H(\omega)| = \begin{cases} 1 & B_1 \leq \omega \leq B_2 \\ 0 & \text{o.w.} \end{cases}$



Ideal Bandstop  $|H(\omega)| = \begin{cases} 0 & B_1 \leq \omega \leq B_2 \\ 1 & \text{o.w.} \end{cases}$



## PHASE FUNCTION

linear phase  $\rightarrow$  no phase distortion.

$\downarrow$

$$\angle H(\omega) = -\omega t_d$$

$\forall \omega$  in passband

$t_d$  - fixed positive delay

if  $\omega_0$  is in passband

$$x(t) = A \cos(\omega_0 t) \xrightarrow{-\infty < t < \infty} y(t) = A |H(\omega_0)| \cos(\omega_0(t - t_d)) \quad -\infty < t < \infty$$

linear phase  $\rightarrow$  time delay of  $t_d$  seconds.

## IDEAL LINEAR PHASE LOWPASS FILTER

$\downarrow$

$$\angle H(\omega) = -\omega t_d$$

$$|\omega| \leq B$$

$$|H(\omega)| = 1 \quad |\omega| \leq B$$

$$H(\omega) = \begin{cases} e^{-j\omega t_d} & |\omega| \leq B \\ 0 & |\omega| > B \end{cases}$$

$$= p_{2B}(\omega) e^{-j\omega t_d} \quad -\infty < \omega < \infty$$

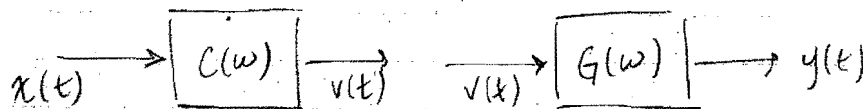
Given  $H(\omega) = p_{2B}(\omega) e^{-j\omega t_d} \xrightarrow{\text{FT.}} h(t) = \frac{B}{\pi} \text{sinc}\left[\frac{B}{\pi}(t - t_d)\right] \quad -\infty < t < \infty$

SEE OTHER SIDE  
FOR DETAILS  
 $H(\omega) \rightarrow h(t)$

$\uparrow$  impulse response of ideal  
lowpass filter (Note: noncausal!)

# 10-15-03 Ch 5 Frequency Domain Analysis.

Note: In channel equalization, we attempt to restore linear phase to corrupted (received) signal.



if  $C(\omega)$  has nonlinear phase (distortion) [RF link?]

then  $v(t)$  may be distorted version of  $x(t)$

design  $G(\omega)$  s.t.

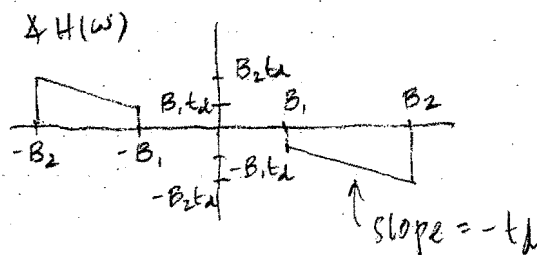
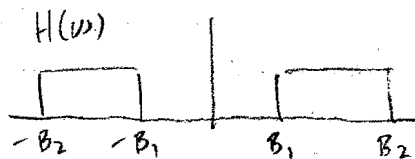
$$C(\omega)G(\omega) = H(\omega)$$

Linear phase

$$G(\omega) = \frac{H(\omega)}{C(\omega)}$$

## IDEAL LINEAR-PHASE BANDPASS FILTER

$$\left. \begin{array}{l} |H(\omega)| = 1 \\ \angle H(\omega) = -\omega t_d \end{array} \right\} \begin{array}{l} B_1 \leq |\omega| \leq B_2 \\ B_1 \leq |\omega| \leq B_2 \\ 0 \text{ o.w.} \end{array}$$



\* See supplemental notes on Response to Nonsinusoidal Input.  
Review during recitation

# 10.15.03 Ch 5 Frequency Domain Analysis

SAMPLING  $x(t) \rightarrow x(nT) \rightarrow x[n]$

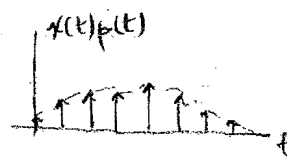
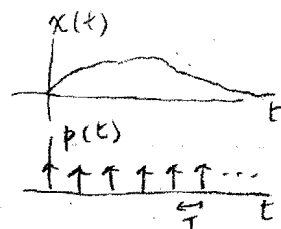
Impulse train  $p(t) = \sum_{n=-\infty}^{\infty} \delta(t-nT)$



$$x(t)p(t) = \sum_{n=-\infty}^{\infty} x(t)\delta(t-nT)$$

$$= \sum_{n=-\infty}^{\infty} x(nT)\delta(t-nT)$$

↑  
T sampling interval



$$x(t)p(t) \xrightarrow{FT} X(\omega) * P(\omega) \quad P(\omega) = ?$$

Note:  $p(t)$  is periodic  $\rightarrow$  Fourier Series.



$$p(t) = \sum_{k=-\infty}^{\infty} c_k e^{jk\omega_s t}$$



$$\omega_s = \frac{2\pi}{T}$$

↑  
sampling frequency  
( $f_s = \frac{1}{T} = \frac{\omega_s}{2\pi}$  Hz)

$$c_k = \frac{1}{T} \int_{-T/2}^{T/2} p(t) e^{-jk\omega_s t} dt$$

$k=0, \pm 1, \pm 2, \dots$  rad/sec

$$= \frac{1}{T} \int_{-T/2}^{T/2} \delta(t) e^{-jk\omega_s t} dt$$

$$= \frac{1}{T} [e^{-jk\omega_s t}]_{t=0}$$

$$= \frac{1}{T}$$

$\delta(t)$  because integral is only over one period.

$$p(t) = \sum_{k=-\infty}^{\infty} \frac{1}{T} e^{jk\omega_s t}$$

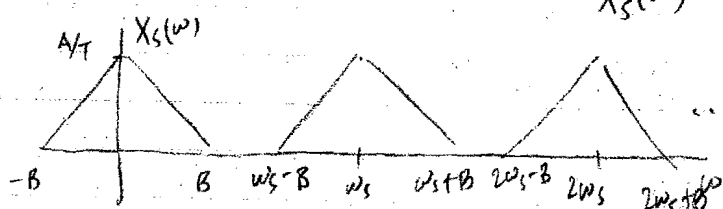
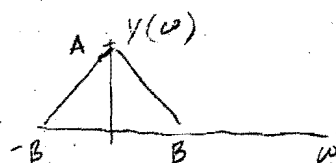
$$\rightarrow x(t)p(t) = \sum_{k=-\infty}^{\infty} \frac{1}{T} x(t) e^{jk\omega_s t}$$

↑  
spectral (frequency)  
modulation



$$X_s(\omega) = X(\omega) * P(\omega) = \sum_{k=-\infty}^{\infty} \frac{1}{T} X(\omega - k\omega_s)$$

Note:  $x_c(t) = x(t)p(t)$



if  $\omega_s - B > B \rightarrow$  NO ALIASING ( $\omega_s > 2B$ )

if  $\omega_s - B < B \rightarrow$  ALIASING ( $\omega_s < 2B$ )

10.15.03 Ch 5 - Frequency Domain Analysis

$\left\{ \begin{array}{l} \text{If } |X(\omega)| = 0 \quad \omega > B \quad \text{strictly band-limited} \\ \downarrow \\ \text{then if } \omega_s \geq 2B \quad x(t) \text{ can be perfectly (exactly) reconstructed from } x_s(t) \text{ (by simple lowpass filtering)} \end{array} \right.$   
 $2B \sim \text{Nyquist sampling freq.}$   
 $\downarrow$   
 INTERPOLATION FILTER  
 $H(\omega) = \begin{cases} T & |\omega| \leq B \\ 0 & \text{o.w.} \end{cases}$   
 $\downarrow$   
 $h(t) = \frac{BT}{\pi} \text{sinc}\left(\frac{B}{\pi}t\right) \quad -\infty < t < \infty$

10.20.03 Ch 7 Discrete-Time Fourier Analysis

✓ Fourier Series<sup>(FS)</sup> - Periodic Waveforms

$$x(t) = x(t+T) \rightarrow x(t) = \sum_{k=-\infty}^{\infty} c_k e^{jk\omega_0 t} \quad -\infty < t < \infty$$

$(\omega_0 = \frac{2\pi}{T})$   
 $\uparrow c_k = \frac{1}{T} \int_{-T/2}^{T/2} x(t) e^{-jk\omega_0 t} dt$

✓ Fourier Transform<sup>(FT)</sup> - Aperiodic Waveforms

$$x(t) \rightarrow X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$$

Discrete-Time Fourier Transform<sup>(DTFT)</sup> - Discrete-time Waveforms

$$x[n] \rightarrow X(\Omega) = \sum_{n=-\infty}^{\infty} x[n] e^{-j\Omega n}$$

Note: Discrete in time / Continuous in frequency ( $\Omega$ )  $\Omega \neq \omega$

DTFT exists if  $x[n]$  is absolutely summable, i.e.,  $\sum_{n=-\infty}^{\infty} |x[n]| < \infty$

Note: any time limited signal satisfies this condition  $\rightarrow \sum_{n=-\infty}^{\infty} |x[n]| = \sum_{n=-N}^N |x[n]| < \infty$

10.20.03 Ch 7 Discrete Time Fourier Analysis

$$X(\Omega) = \sum_{n=-\infty}^{\infty} x[n] e^{-j\Omega n} \quad (e^{-jn2\pi} = 1 \text{ all integers } n)$$

↑ periodic fn of  $\Omega$  w/ period  $2\pi$ .  $\rightarrow X(\Omega + 2\pi) = X(\Omega)$

$\therefore X(\Omega)$  is completely determined over any  $2\pi$  interval

$$0 \leq \Omega \leq 2\pi \quad \swarrow \quad -\pi \leq \Omega \leq \pi$$

$X(\Omega)$  complex-valued in general,

$$X(\Omega) = R(\Omega) + jI(\Omega)$$

$$= \sum x[n] e^{-j\Omega n}$$

$$= \sum x[n] (\cos(\Omega n) - j \sin(\Omega n))$$

$$= \sum_{n=-\infty}^{\infty} x[n] \cos(\Omega n) + j \left( -\sum_{n=-\infty}^{\infty} x[n] \sin(\Omega n) \right)$$

$$\begin{cases} R(\Omega) = \sum_{n=-\infty}^{\infty} x[n] \cos(\Omega n) \\ I(\Omega) = -\sum_{n=-\infty}^{\infty} x[n] \sin(\Omega n) \end{cases}$$

$$|X(\Omega)| = (R^2(\Omega) + I^2(\Omega))^{1/2}$$

$$\angle X(\Omega) = \tan^{-1} \left( \frac{I(\Omega)}{R(\Omega)} \right)$$

$$X(\Omega) = |X(\Omega)| e^{j\angle X(\Omega)}$$

$|X(\Omega)|$  &  $\angle X(\Omega)$  are periodic in  $\Omega$   
 $\therefore$  need be defined over  $2\pi$  interval.

If  $x[n]$  is real-valued  $\rightarrow |X(-\Omega)| = |X(\Omega)|$

$$\angle X(-\Omega) = -\angle X(\Omega)$$

If  $x[n]$  is even ( $x[-n] = x[n]$ )  $\rightarrow X(\Omega) = x[0] + 2 \sum_{n=1}^{\infty} x[n] \cos(\Omega n)$

If  $x[n]$  is odd ( $x[-n] = -x[n]$ )  $\rightarrow X(\Omega) = -2j \sum_{n=1}^{\infty} x[n] \sin(\Omega n)$

10.22.03 Ch 7 Discrete-Time Fourier Analysis

$$X(\Omega + 2\pi) = X(\Omega)$$

throughout text  $\rightarrow$  use interval  $-\pi \leq \Omega \leq \pi$

remember  $\Omega \neq \omega$  highest frequency in DTFT is at  $\pm\pi$  (i.e.  $\Omega = \pm\pi$ )

Must recognize - FT  $-\infty < \omega < \infty$   
DTFT  $-\pi \leq \Omega \leq \pi$

Sampling interval  $T$   
is normalized to unity  
(actual frequency range  
is function of samp. freq.  $= 1/T$ )  
 $-\pi = -f/2$      $\pi = f/2$

INVERSE DTFT

$$x[n] = \frac{1}{2\pi} \int_0^{2\pi} X(\Omega) e^{j\Omega n} d\Omega$$
$$= \frac{1}{2\pi} \int_{-\pi}^{\pi} X(\Omega) e^{j\Omega n} d\Omega$$

PROPERTIES OF DTFT - see Tables 7.1 & 7.2 pp 308-309

10.27.03

DISCRETE FOURIER TRANSFORM (DFT)

$\uparrow$   
DISCRETE IN TIME  
DISCRETE IN FREQUENCY

given  $x[n] = 0$   $n < 0$  &  $n \geq N$

$N$ -pt DFT of  $x[n] \rightarrow X_k = \sum_{n=0}^{N-1} x[n] e^{-j\frac{2\pi kn}{N}}$   $k=0, 1, \dots, N-1$

$\{X_0, X_1, \dots, X_{N-1}\}$  completely represent  $x[n]$

$\uparrow$   
Complex Valued  $\rightarrow X_k = |X_k| e^{j\angle X_k}$   
 $= R_k + jI_k$

DFT always exists since  $\sum_{n=0}^{N-1} |x[n]| < \infty$

10.27.03 Ch 7 Discrete Time Fourier Analysis

INVERSE DFT 
$$x[n] = \frac{1}{N} \sum_{k=0}^{N-1} X_k e^{j2\pi kn/N} \quad n=0,1,\dots,N-1$$

RELATION TO DTFT

$$X_k = X(\Omega) \Big|_{\Omega = \frac{2\pi k}{N}} = X\left(\frac{2\pi k}{N}\right) \quad k=0,1,\dots,N-1$$

4.11

Go over Examples ~~4.10~~ and 7.11 in text.

DFT OF TRUNCATED SIGNAL

$$\tilde{x}[n] = \begin{cases} x[n] & n=0,1,\dots,N-1 \\ 0 & n \geq N \end{cases}$$

if  $p[n - \frac{N-1}{2}] = \begin{cases} 1 & n=0,1,\dots,N-1 \\ 0, \text{w.} & \end{cases}$

then  $\tilde{x}[n] = x[n] \cdot p[n - \frac{N-1}{2}]$

$\Downarrow$

$$\tilde{X}(\Omega) = X(\Omega) * P(\Omega)$$

$$\tilde{X}_k = [X(\Omega) * P(\Omega)]_{\Omega = \frac{2\pi k}{L}} \quad k=0,1,\dots,L-1$$

$\uparrow$  L-pt DFT of  $\tilde{x}[n]$

skip.

SYSTEM ANALYSIS VIA DTFT/DFT

$$y[n] = x[n] * h[n] = \sum_{i=-\infty}^{\infty} h[i] x[n-i]$$

assuming  $h[n]$  is absolutely summable  $(\sum_{n=-\infty}^{\infty} |h[n]| < \infty)$

$$H(\Omega) = \sum_{n=-\infty}^{\infty} h[n] e^{-j\Omega n}$$

$$\rightarrow Y(\Omega) = H(\Omega) X(\Omega)$$

$$|Y(\Omega)| = |H(\Omega)| |X(\Omega)| \quad \angle Y(\Omega) = \angle H(\Omega) + \angle X(\Omega)$$



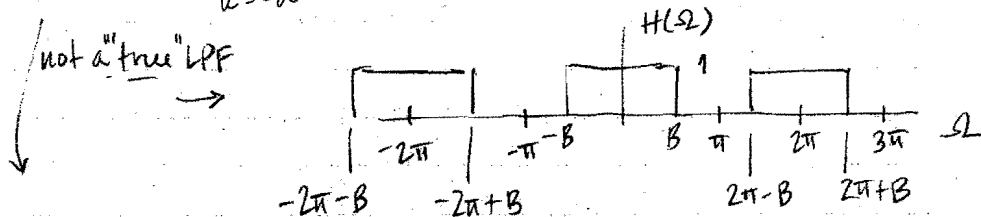
10.27.03 Ch 7 Discrete Time Fourier Analysis.

RESPONSE TO SINUSOIDAL INPUT

$$x[n] = A \cos(\Omega_0 n + \theta) \quad n = 0, \pm 1, \pm 2, \dots$$

$$y[n] = A |H(\Omega_0)| \cos(\Omega_0 n + \theta + \angle H(\Omega_0)) \quad \Omega_0 \geq 0$$

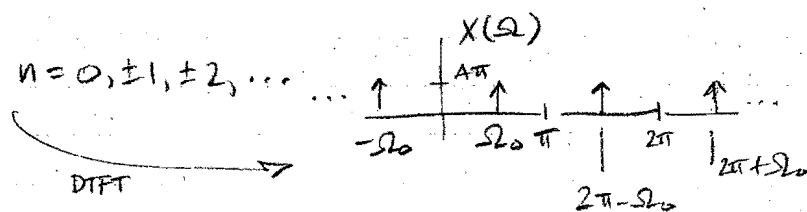
Suppose  $H(\Omega) = \sum_{k=-\infty}^{\infty} p_{2B}(\Omega + 2\pi k)$  periodic in  $2\pi$



given  $x[n] = A \cos(\Omega_0 n)$   $n = 0, \pm 1, \pm 2, \dots$

$$y[n] = x[n] * h[n]$$

$$Y(\Omega) = X(\Omega) H(\Omega)$$



if  $\Omega_0 \leq B \rightarrow Y(\Omega) = X(\Omega) H(\Omega) = X(\Omega) \rightarrow y[n] = x[n] = A \cos(\Omega_0 n)$

if  $B < \Omega_0 < \pi \rightarrow Y(\Omega) = X(\Omega) H(\Omega) = 0 \rightarrow y[n] = 0$

$\therefore y[n] = A \cos(\Omega_0 n)$  if  $2\pi k - B \leq \Omega_0 \leq 2\pi k + B$

F1 - unit-pulse response of  $H(\Omega) = \sum_{k=-\infty}^{\infty} p_{2B}(\Omega + 2\pi k)$

$$h[n] = \frac{B}{\pi} \text{sinc}\left(\frac{B}{\pi} n\right) \quad n = 0, \pm 1, \pm 2, \dots$$

$h[n] \sim$  noncausal  $\rightarrow$  no real-time implementation

$\rightarrow$  operate off-line on stored and current data.

## DFT SYSTEM ANALYSIS

$$\left\{ \begin{array}{l} \text{if } x[n] = 0 \quad n < 0 \text{ and } n \geq N \\ \text{and } h[n] = 0 \quad n < 0 \text{ and } n > Q \end{array} \right.$$

$$\begin{aligned} \text{then } y[n] &= h[n] * x[n] = \sum_{i=0}^{\infty} h[i] x[n-i] \quad n \geq 0 \\ &= \sum_{i=0}^Q h[i] x[n-i] \quad n \geq 0 \end{aligned}$$

$$y[n] = 0 \quad \text{all } n \geq N+Q$$

In DFT domain - pad  $x[n]$  &  $h[n]$  to length  $N+Q$   
 $\uparrow$   
 zero

$$\begin{aligned} \rightarrow \quad x[n] &= 0 \quad n = N, N+1, \dots, N+Q-1 \\ h[n] &= 0 \quad n = Q, Q+1, \dots, N+Q-1 \end{aligned}$$

$\Downarrow$   $(N+Q)$ -pt DFTs

$$X_k = \sum_{n=0}^{N+Q-1} x[n] e^{-j2\pi kn/(N+Q)} \quad k = 0, 1, \dots, N+Q-1$$

$$H_k = \sum_{n=0}^{N+Q-1} h[n] e^{-j2\pi kn/(N+Q)} \quad k = 0, 1, \dots, N+Q-1$$

$\downarrow$

$$Y_k = H_k X_k \quad k = 0, 1, \dots, N+Q-1$$

$$\text{IDFT} \rightarrow y[n] = \frac{1}{N+Q} \sum_{k=0}^{N+Q-1} H_k X_k e^{j2\pi kn/(N+Q)} \quad n = 0, 1, \dots, N+Q-1$$

if  $x[n] \neq 0 \quad n \geq N$  and/or  $h[n] \neq 0 \quad n > Q$

$y[n]$  is only approximate expression

10-29-03 Ch 8 - Laplace Transform.

$$\text{FT } X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$$

For existence,  $x(t)$  must be absolutely integrable.

If  $x(t) = u(t) \rightarrow$  not absolutely integrable  
no Fourier Transform (in ordinary sense)

$$\therefore X(\omega) = \int_0^{\infty} e^{-j\omega t} dt \quad \text{does not exist!} \\ (e^{-j\omega \infty} = ?)$$

If  $x(t) = e^{-\sigma t} u(t) \rightarrow$  absolutely integrable  
if  $\sigma > 0$

$$\rightarrow \text{F.T. exists. } X(\omega) = \int_0^{\infty} e^{-\sigma t} e^{-j\omega t} dt \\ = \int_0^{\infty} e^{-(\sigma + j\omega)t} dt$$

$$\text{let } s = \sigma + j\omega \rightarrow X(s) = \int_0^{\infty} e^{-st} dt$$

$\uparrow$   
complex  
number

$\uparrow$

$$= \frac{1}{s}$$

Laplace Transform  
of unit-step fn.

$\uparrow$   
complex-valued.

$$X(s) = \frac{1}{s}$$

defined only for  $\text{Re}\{s\} = \sigma > 0$   
(not defined for  $\sigma = 0$  or  $\sigma < 0$ )

$\text{Re}\{s\} = \sigma > 0$  Region of Convergence

In general

$$X(s) = \int_0^{\infty} x(t) e^{-st} dt$$

the set of all complex numbers  $s$  for which  $X(s)$   
exists is REGION of CONVERGENCE

$\uparrow$   
depends on given fn  $x(t)$

10.29.03 Ch 8 - Laplace Transform

if  $x(t) = e^{-bt} u(t)$

↓

$$\begin{aligned}\text{then } X(s) &= \int_0^{\infty} e^{-bt} e^{-st} dt \\ &= \int_0^{\infty} e^{-(b+s)t} dt \\ &= -\frac{1}{(s+b)} \left[ e^{-(s+b)t} \right]_{t=0}^{t=\infty}\end{aligned}$$

What is limit  $e^{-(s+b)t}$  as  $t \rightarrow \infty$ ?

$$e^{-(s+b)t} = e^{-(\sigma+j\omega+b)t} \rightarrow 0 \text{ as } t \rightarrow \infty$$

if  $\sigma+b > 0$

↓

$$\text{ROC: } \operatorname{Re}\{s\} = \sigma > -b$$

$$\text{As such } \rightarrow X(s) = \frac{1}{s+b} \leftrightarrow x(t) = e^{-bt} u(t)$$

Relationship b/w Fourier Transform + Laplace Transform

$$X(\omega) = X(s) \Big|_{s=j\omega} \text{ valid iff } \sigma=0 \in \text{ROC of } X(s)$$

### PROPERTIES OF LAPLACE TRANSFORM

LINEARITY  $ax(t) + bv(t) \leftrightarrow aX(s) + bV(s)$

RIGHT TIME SHIFT  $x(t-c)u(t-c) \leftrightarrow e^{-cs}X(s)$

TIME SCALING  $x(at) \leftrightarrow \frac{1}{a} X\left(\frac{s}{a}\right)$

MULTIPLICATION by POWER of  $t$   $t^N x(t) \leftrightarrow (-1)^N \frac{d^N}{ds^N} X(s)$

MULT BY EXPONENTIAL

$$e^{at} x(t) \leftrightarrow X(s-a)$$

SIN

$$x(t) \sin \omega t \leftrightarrow \frac{1}{2j} [X(s+j\omega) - X(s-j\omega)]$$

COS

$$x(t) \cos \omega t \leftrightarrow \frac{1}{2} [X(s+j\omega) + X(s-j\omega)]$$

# 10.29.03 Ch 8 Laplace Transform

## DIFFERENTIATION IN TIME

$$\dot{x}(t) \leftrightarrow sX(s) - x(0)$$

$$\frac{d^N}{dt^N} x(t) = x^{(N)}(t) \leftrightarrow s^N X(s) - s^{N-1} x(0) - s^{N-2} \dot{x}(0) - \dots - s x^{(N-2)}(0) - x^{(N-1)}(0)$$

## INTEGRATION

$$\int_0^t x(\lambda) d\lambda \leftrightarrow \frac{1}{s} X(s)$$

## CONVOLUTION

$$x(t) * v(t) \leftrightarrow X(s) V(s)$$

INITIAL VALUE THM -  $x(0) = \lim_{s \rightarrow \infty} sX(s)$   
 (valid for  $t=0, 0^+$ )  
NOT for  $t=0^-$

$$\dot{x}(0) = \lim_{s \rightarrow \infty} [s^2 X(s) - s x(0)]$$

$$x^{(N)}(0) = \lim_{s \rightarrow \infty} [s^{N+1} X(s) - s^N x(0) - s^{N-1} \dot{x}(0) - \dots - s x^{(N-2)}(0)]$$

## FINAL VALUE THM

$$\lim_{t \rightarrow \infty} x(t) = \lim_{s \rightarrow 0} sX(s)$$

## Inverse Laplace Transform

$$x(t) = \frac{1}{2\pi j} \int_{c-j\infty}^{c+j\infty} X(s) e^{st} ds$$

$c$  is any real number for which the path from  $s = c - j\infty$  to  $s = c + j\infty$  lies in the ROC of  $X(s)$

In practice, we seldom actually evaluate this integral  
 ↓ - require a course in COMPLEX VARIABLES

Instead - we'll use Partial Fraction Expansion & known Laplace Transform pairs (for rational  $X(s)$  - explained now)

# 11.3.03 Ch8. Laplace Transforms.

Suppose  $x(t) \rightarrow X(s) = \frac{B(s)}{A(s)} = \frac{b_M s^M + b_{M-1} s^{M-1} + \dots + b_1 s + b_0}{a_N s^N + a_{N-1} s^{N-1} + \dots + a_1 s + a_0}$

$$\{b_M, \dots, b_0, a_N, \dots, a_0\} \in \mathbb{R}$$

$M, N \in \text{positive integers.}$

if  $b_M \neq 0 \rightarrow B(s) \sim \text{degree } M$   
 if  $a_N \neq 0 \rightarrow A(s) \sim \text{degree } N$

(Note: assumed factors  $(s-k)$  common to  $B(s)$  &  $A(s)$  are already factored out)

$X(s) = \frac{B(s)}{A(s)}$  "rational fn of  $s$ " of order  $N$

roots of denominator ( $A(s)$ ) are values of  $s$  for which

$A(s) = 0$  as such  $A(s) = a_N (s-p_1)(s-p_2)\dots(s-p_N)$

"zeros" of  $A(s) \rightarrow \{p_1, p_2, \dots, p_N\} \in \mathbb{R} \text{ or } \mathbb{C}$

$\uparrow$  poles of  $X(s) = \text{zeros of } A(s)$

Note: complex zeros (poles) occur in complex conjugate pairs.

Use MATLAB to determine roots of arbitrary  $A(s)$  - complex conjugate pairs.

$$X(s) = \frac{B(s)}{a_N (s-p_1)(s-p_2)\dots(s-p_N)}$$

poles of  $X(s) = \text{zeros of } A(s)$   
 $\downarrow$  make  $X(s) \rightarrow \infty$   $\downarrow$  make  $A(s) \rightarrow 0$

if  $M < N \rightarrow X(s)$  is strictly proper in  $s$

DISTINCT POLES (NON-REPEATING)  $\rightarrow p_i \neq p_j, i \neq j$

PFE  $\rightarrow$   
 partial fraction  
 expansion.

$$X(s) = \frac{C_1}{s-p_1} + \frac{C_2}{s-p_2} + \dots + \frac{C_N}{s-p_N} \quad \text{w/ } C_i = \left[ (s-p_i) X(s) \right]_{s=p_i}$$

$\{C_i\} \ i=1, 2, \dots, N \sim \text{RESIDUES of } X(s)$   $i=1, 2, \dots, N$

11.3.03 Ch 8 Laplace Transform.

$c_i$  is real if  $p_i$  is real      complex  $c_i$  occur in complex conjugate pairs. (result of  $p_i \neq \bar{p}_i$ )

Note: to compute  $\{c_i\} = \left\{ \left[ (s-p_i)X(s) \right]_{s=p_i} \right\}$   
do not need to factor  $B(s)$ .  
(you do need to factor  $A(s)$  to resolve poles)

$$X(s) = \frac{c_1}{s-p_1} + \frac{c_2}{s-p_2} + \dots + \frac{c_N}{s-p_N}$$

$\downarrow \mathcal{L}^{-1}\{ \cdot \}$

$$x(t) = c_1 e^{p_1 t} + c_2 e^{p_2 t} + \dots + c_N e^{p_N t} \quad t \geq 0$$

↑ ↗

poles determine convergence properties of  $x(t)$   
 each term represents a "mode" of convergence  
 - if  $\Re(p_i) > 0 \rightarrow$  that mode grows w/o bound  
 - stability (studied later) requires  $\Re(p_i) < 0 \quad \forall i$   
 -  $\Re(p_i) = 0 \rightarrow$  marginally stable  
 poles  $\in$  LHP of s-plane

poles determine characteristics of the time variation of  $x(t)$

if  $c_i(p_i)$  are real  $\rightarrow c_i e^{p_i t}$  is real

if  $c_i(p_i)$  are complex  $\rightarrow c_i e^{p_i t} \& \bar{c}_i e^{\bar{p}_i t}$   
 can be combined to produce real form.

DISTINCT POLES w/ TWO OR MORE COMPLEX POLES.  
 (SHU distinct)

suppose  $p_1 = \sigma + j\omega$  ( $\omega \neq 0$ )  $\rightarrow \bar{p}_1 = \sigma - j\omega$  is also a pole.

$\{p_1, \bar{p}_1\}$   
 $\downarrow$   
 $\{c_1, \bar{c}_1\}$

$$\hookrightarrow X(s) = \frac{c_1}{s-p_1} + \frac{\bar{c}_1}{s-\bar{p}_1} + \frac{c_3}{s-p_3} + \dots + \frac{c_N}{s-p_N}$$

$\downarrow \mathcal{L}^{-1}\{ \cdot \}$

$$x(t) = c_1 e^{p_1 t} + \bar{c}_1 e^{\bar{p}_1 t} + c_3 e^{p_3 t} + \dots + c_N e^{p_N t} \quad t \geq 0$$

$$\rightarrow \rightarrow = 2|c_1| e^{\sigma t} \cos(\omega t + \phi_{c_1}) + c_3 e^{p_3 t} + \dots + c_N e^{p_N t}$$

$$c_1 e^{p_1 t} + \bar{c}_1 e^{\bar{p}_1 t} = 2|c_1| e^{\sigma t} \cos(\omega t + \phi_{c_1})$$

11.3.03 Ch 8. Laplace Transform.

6.17 6.18

Examples 8.16 & 8.17 are pretty good demonstrations.

Alternative means of resolving complex poles -

$$\text{suppose } X(s) = \frac{b_1 s + b_0}{s^2 + a_1 s + a_0}$$

↓ "completing the square"

$$X(s) = \frac{b_1 s + b_0}{(s + \frac{a_1}{2})^2 + a_0 - \frac{a_1^2}{4}}$$

(remember:  $M < N$ )

poles of  $X(s)$  are complex (a la quadratic formula) iff  $a_0 - \frac{a_1^2}{4} > 0$ .

$$\text{if } a_0 - \frac{a_1^2}{4} > 0 \rightarrow p_1, \bar{p}_1 = -\frac{a_1}{2} \pm j\omega \quad \omega / \omega = (a_0 - \frac{a_1^2}{4})^{1/2}$$

↓

$$X(s) = \frac{b_1 s + b_0}{(s + \frac{a_1}{2})^2 + \omega^2} = \frac{b_1 (s + \frac{a_1}{2})}{(s + \frac{a_1}{2})^2 + \omega^2} + \frac{(b_0 - b_1 \frac{a_1}{2}) \cdot \frac{1}{\omega} \cdot \omega}{(s + \frac{a_1}{2})^2 + \omega^2}$$

from look-up table

$$x(t) = b_1 e^{-\frac{a_1 t}{2}} \cos(\omega t) u(t) + (b_0 - \frac{b_1 a_1}{2}) \cdot \frac{1}{\omega} e^{-\frac{a_1 t}{2}} \sin(\omega t) u(t)$$

↑ keep eye on this

In general, suppose

$$X(s) = \frac{B(s)}{[(s-\sigma)^2 + \omega^2](s-p_3)(s-p_4)\dots(s-p_n)}$$

$$= \frac{b_1 s + b_0}{(s-\sigma)^2 + \omega^2} + \frac{c_3}{s-p_3} + \frac{c_4}{s-p_4} + \dots + \frac{c_n}{s-p_n} \quad \{b_0, b_1, c_3, c_4, \dots, c_n\} \in \mathbb{R}$$

$b_1$  &  $b_0$  could be determined by putting RHS above over common denominator

$$[(s-\sigma)^2 + \omega^2](s-p_3)(s-p_4)\dots(s-p_n)$$

and equating terms

(Example 6.20 8.19 in text)



# 11.10.03 Ch 8 Laplace Transform

## REPEATED POLES ( $M < N$ )

$$X(s) = \frac{B(s)}{A(s)} = \frac{B(s)}{(s-p_1)^r (s-p_{r+1}) \dots (s-p_N)}$$

↑ repeated  $r$  times

$$X(s) = \frac{c_1}{(s-p_1)} + \frac{c_2}{(s-p_1)^2} + \dots + \frac{c_r}{(s-p_1)^r} + \frac{c_{r+1}}{(s-p_{r+1})} + \dots + \frac{c_N}{(s-p_N)}$$

$$\{c_1, \dots, c_r\} \rightarrow c_{r-i} = \frac{1}{i!} \left[ \frac{d^i}{ds^i} [(s-p_1)^r X(s)] \right]_{s=p_1}$$

$i = 0, 1, 2, \dots, r-1$

$$\therefore c_r = [(s-p_1)^r X(s)]_{s=p_1}$$

$$c_{r-1} = \left[ \frac{d}{ds} [(s-p_1)^r X(s)] \right]_{s=p_1}$$

Note:  $t^N e^{-bt} u(t) \leftrightarrow \frac{N!}{(s+b)^{N+1}}$   
 $N = 1, 2, 3, \dots$

$\{c_1, \dots, c_r\}$  could also be determined by

- evaluating coefficients (w/ common denominator & linear alg.)
- quadratic terms

If  $M \geq N$

$$\rightarrow X(s) = \frac{B(s)}{A(s)} = Q(s) + \frac{R(s)}{A(s)}$$

↑ degree  $M-N$       ↑ expand using PFE

## TRANSFORM OF INPUT/OUTPUT DIFF EQS

1<sup>st</sup> ORDER CASE  $\frac{dy(t)}{dt} + ay(t) = bx(t)$

↓  $\mathcal{L}\{\}$     ↓  $\mathcal{L}\{\}$     ↓  $\mathcal{L}\{\}$

$$sY(s) - y(0) + aY(s) = bX(s)$$

$$\therefore (s+a)Y(s) = y(0) + bX(s)$$

$$\rightarrow Y(s) = \frac{y(0)}{(s+a)} + \frac{b}{(s+a)} X(s)$$

# 11.10.03 Ch 8 Laplace Transform

$$Y(s) = \frac{y(0^-)}{(s+a)} + \frac{b}{(s+a)} X(s)$$

↑  
output due to  
initial condition

↑  
output due to  
forcing fn.  $x(t)$

$$[x(t) = \delta(t) \rightarrow X(s) = 1]$$

if no initial energy  $\rightarrow y(0^-) = 0 \rightarrow Y(s) = \frac{b}{(s+a)} X(s)$   
 $= H(s) X(s)$

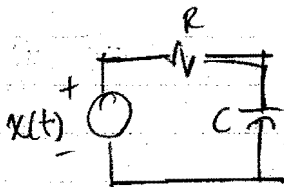
$$H(s) = \frac{b}{s+a} \text{ transfer fn.}$$

$$\downarrow$$
  

$$h(t) = be^{-at} u(t)$$

In general,

$$H(s) = \frac{Y(s)}{X(s)} \text{ transfer fn representation}$$



$$\rightarrow \frac{dy(t)}{dt} + \frac{1}{RC} y(t) = \frac{1}{RC} x(t)$$

$$(s + \frac{1}{RC}) Y(s) = y(0^-) + \frac{1}{RC} X(s)$$

$$\rightarrow Y(s) = \frac{y(0^-)}{(s + \frac{1}{RC})} + \frac{(1/RC) X(s)}{(s + \frac{1}{RC})}$$

if  $x(t) = u(t) \rightarrow X(s) = \frac{1}{s} \rightarrow$  final  $y(t) = y(0^-) e^{-(1/RC)t} + 1 - e^{-(1/RC)t} \quad t \geq 0$

## SECOND-ORDER CASE

$$\frac{d^2 y(t)}{dt^2} + a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_1 \frac{dx(t)}{dt} + b_0 x(t)$$

$$\downarrow \quad \downarrow \quad \downarrow \quad \downarrow$$

$$s^2 Y(s) - sy(0^-) - \dot{y}(0^-) + a_1 s Y(s) - a_1 y(0^-) + a_0 Y(s) = b_1 s X(s) - b_1 x(0^-) + b_0 X(s)$$

$$Y(s) = \frac{y(0^-)s + \dot{y}(0^-) + a_1 y(0^-)}{s^2 + a_1 s + a_0} + \frac{b_1 s + b_0}{s^2 + a_1 s + a_0} X(s)$$

iff  $y(0^-) = \dot{y}(0^-) = 0$

then

$$H(s) = \frac{b_1 s + b_0}{s^2 + a_1 s + a_0}$$

$$Y(s) = H(s) X(s)$$

11.10.03 ch 8 Laplace Transform.

$$N^{\text{th}} \text{ ORDER CASE} - \frac{d^N y(t)}{dt^N} + \sum_{i=0}^{N-1} a_i \frac{d^i y(t)}{dt^i} = \sum_{j=0}^M b_j \frac{d^j x(t)}{dt^j} \quad M \leq N$$

assuming  $y(0^-) = \dot{y}(0^-) = \dots = y^{(N-1)}(0^-) = 0 \rightarrow$

$$Y(s) = \underbrace{\frac{b_M s^M + \dots + b_1 s + b_0}{s^N + a_{N-1} s^{N-1} + \dots + a_1 s + a_0}}_{H(s)} X(s)$$

TRANSFER FN. REPRESENTATION

$$y(t) = h(t) * x(t) = \int_0^\infty h(\lambda) x(t-\lambda) d\lambda$$

$$\downarrow$$

$$Y(s) = H(s) X(s) \quad (h(t) \leftrightarrow H(s))$$

$$\downarrow$$

$$H(s) = \frac{Y(s)}{X(s)} \quad \text{valid iff system is LTI}$$

if not LTI  $H(s)$  would have no meaning

- vary in time
- nonlinear effects

Any system given by input/output diff eq.  
 $\rightarrow$  yields transfer fn ( $H(s)$ ) ~ rational fn of  $s$ .

$$H(s) = \frac{b_M s^M + \dots + b_1 s + b_0}{s^N + a_{N-1} s^{N-1} + \dots + a_1 s + a_0}$$

$\swarrow$   
 (leading denominator coefficient is 1)

$$H(s) = \frac{b_M (s-z_1)(s-z_2)\dots(s-z_M)}{(s-p_1)(s-p_2)\dots(s-p_N)}$$

$\swarrow$   $\{z_1, z_2, \dots, z_M\}$  - ZEROS.

$\swarrow$   $\{p_1, p_2, \dots, p_N\}$  - POLES.

R/LC CIRCUITS

—  $v(t) = R i(t) \rightarrow V(s) = R I(s)$

—  $\frac{dv(t)}{dt} = \frac{1}{C} i(t) \rightarrow sV(s) - v(0) = \frac{1}{C} I(s)$

$$V(s) = \frac{1}{Cs} I(s) + \frac{1}{s} v(0)$$

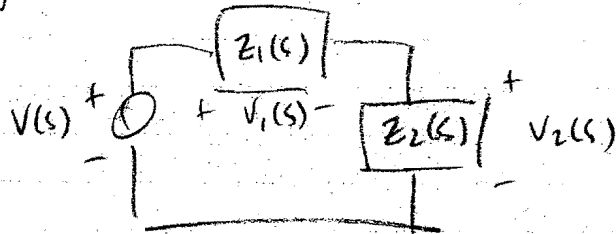
—  $v(t) = L \frac{di(t)}{dt} \rightarrow V(s) = sLI(s) - Li(0)$

shuf.

# 11.10.03 Ch 8 Laplace Transforms

Resistor Impedance  $\rightarrow R$   
 Capacitor Impedance  $\rightarrow 1/s$   
 Inductor Impedance  $\rightarrow sL$

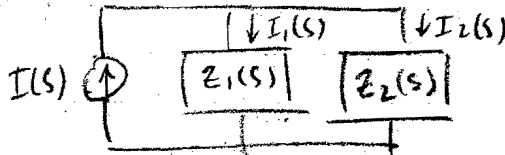
Voltage Divider -



$$V_1(s) = \frac{Z_1(s)}{Z_1(s) + Z_2(s)} V(s)$$

$$V_2(s) = \frac{Z_2(s)}{Z_1(s) + Z_2(s)} V(s)$$

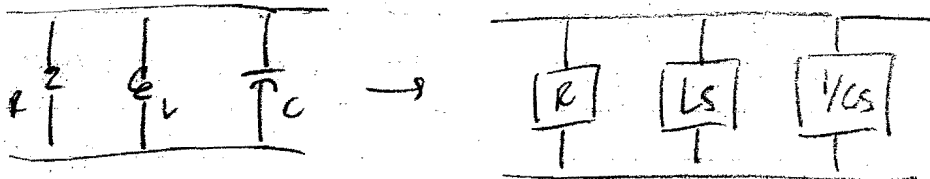
Current Divider



$$I_1(s) = \frac{Z_2(s)}{Z_1(s) + Z_2(s)} I(s)$$

$$I_2(s) = \frac{Z_1(s)}{Z_1(s) + Z_2(s)} I(s)$$

$R \parallel L \parallel C$  det



Integrators  $\rightarrow y(t) = y(0) + \int_0^t x(t) dt$   $\xrightarrow{x(t)} \boxed{\int dt} \xrightarrow{y(t)}$

$$Y(s) = \frac{1}{s} y(0) + \frac{1}{s} X(s)$$

if  $y(0) = 0 \rightarrow Y(s) = \frac{1}{s} X(s)$

$$X(s) \rightarrow \boxed{\frac{1}{s}} \rightarrow Y(s)$$

↑ INTEGRATE  
 ↓ DERIVATIVE

Differentiator  $\rightarrow y(t) = \frac{dx(t)}{dt}$   $\xrightarrow{x(t)} \boxed{\frac{d}{dt}} \rightarrow y(t)$

$$Y(s) = sX(s) - x(0)$$

if  $x(0) = 0 \rightarrow Y(s) = sX(s)$   $X(s) \rightarrow \boxed{s} \rightarrow Y(s)$

11.12.03 Ch 9 Transfer fn - System Anal.  
(9.1, 9.4, 9.5)

$$L(s) = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_1 s + b_0}{s^N + a_{N-1} s^{N-1} + \dots + a_1 s + a_0}$$

↑  
stability requires  $\rightarrow \operatorname{Re}\{p_i\} < 0 \quad i=1,2,\dots,N$

$\therefore h(t)$  converges to 0 as  $t \rightarrow \infty$  iff  $\forall p_i \in \text{OLHP}$

⇔

stable if  $h(t) \rightarrow 0$   
as  $t \rightarrow \infty$

(open left-half plane)

marginally stable if  $|h(t)| \leq c$  for all  $t$

$\rightarrow \operatorname{Re}\{p_i\} \leq 0 \quad i=1,2,\dots,N$

↓  
 $\therefore$  can be poles (nonrepeated) on  $j\omega$  axis.

unstable  $|h(t)| \rightarrow \infty$  as  $t \rightarrow \infty$

$\therefore$  at least 1 pole is in ORHP  
or repeated poles on  $j\omega$ -axis.

Other models of stability -

\*  $h(t) \rightarrow 0$  as  $t \rightarrow \infty$  iff  $\int_0^\infty |h(t)| dt < \infty$   
absolute integrability

\* BIBO stable (bounded input  $\rightarrow$  bounded output)  
if  $|x(t)| \leq c_1 \rightarrow |y(t)| \leq c_2 \quad \forall t$

BIBO stable  $\equiv$  absolute integrability.

↓ skip.

11-12-03 Ch 9 - Transfer fn - System Analysis.

$$H(s) = \frac{B(s)}{A(s)}$$

$$x(t) = C \cos \omega_0 t \quad t \geq 0$$

$$\downarrow$$

$$X(s) = \frac{Cs}{s^2 + \omega_0^2} = \frac{Cs}{(s+j\omega_0)(s-j\omega_0)} \quad \begin{matrix} \rightarrow \text{zero @ } s=0 \\ \rightarrow \text{poles @ } s = \pm j\omega_0 \end{matrix}$$

assuming no initial energy  $\rightarrow Y(s) = H(s)X(s)$

$$= \frac{B(s)}{A(s)} \cdot \frac{Cs}{(s+j\omega_0)(s-j\omega_0)}$$

$$= \frac{r(s)}{A(s)} + \frac{c}{s-j\omega_0} + \frac{\bar{c}}{s+j\omega_0}$$

$r(s)$  is polynomial in  $s$

$$c = [(s-j\omega_0) Y(s)] \Big|_{s=j\omega_0}$$

$$= \left[ \frac{Cs B(s)}{A(s)(s+j\omega_0)} \right]_{s=j\omega_0}$$

$$= \frac{jC\omega_0 B(j\omega_0)}{A(j\omega_0)(j2\omega_0)}$$

$$= \frac{C}{2} H(j\omega_0) \quad \rightarrow \quad Y(s) = \frac{r(s)}{A(s)} + \frac{(\frac{C}{2}) H(j\omega_0)}{(s-j\omega_0)} + \frac{(\frac{C}{2}) \overline{H(j\omega_0)}}{(s+j\omega_0)}$$

$$\downarrow \quad \downarrow$$

$$y(t) = y_1(t) + \frac{C}{2} H(j\omega_0) e^{j\omega_0 t} + \frac{C}{2} \overline{H(j\omega_0)} e^{-j\omega_0 t}$$

$$= y_1(t) + C |H(j\omega_0)| \cos(\omega_0 t + \angle H(j\omega_0))$$

if system is stable  $\rightarrow y_1(t) \rightarrow 0$  as  $t \rightarrow \infty$  }  $y_1(t)$  is transient response  $t \geq 0$

steady-state:  $y_{ss}(t) = C |H(j\omega_0)| \cos(\omega_0 t + \angle H(j\omega_0)) \quad t \geq 0$

$$H(j\omega) = H(\omega) \quad \rightarrow \quad y_{ss}(t) = C |H(\omega_0)| \cos(\omega_0 t + \angle H(\omega_0)) \quad t \geq 0$$

$\therefore$  frequency response of stable system can be determined from  $H(s)$

11-17-03 Ch 9 Transfer fn - System Anal.

Arbitrary Input

$$X(s) = \frac{C(s)}{D(s)}$$

$$H(s) = \frac{B(s)}{A(s)}$$

$$Y(s) = H(s)X(s) = \frac{B(s)C(s)}{A(s)D(s)}$$

↓

$$= \frac{E(s)}{A(s)} + \frac{F(s)}{D(s)}$$

↓

↓

$$y(t) = y_1(t) + y_2(t)$$

↑

↑

form depends  
on poles of  $H(s)$

form depends on  
poles of  $X(s)$

if  $H(s)$  is stable  
 $y_1(t) \rightarrow 0$   
as  $t \rightarrow \infty$

if  $X(s)$  has poles  
on  $j\omega$ -axis  
 $y_2(t) \not\rightarrow 0$  as  $t \rightarrow \infty$

TRANSIENT RESPONSE

STEADY-STATE RESPONSE

Frequency Response Function

rational transfer fn.  $H(s) = \frac{B(s)}{A(s)}$

given  $x(t) = C \cos(\omega_0 t)$   $t \geq 0$ .

↓

$$y_{ss}(t) = C |H(\omega_0)| \cos(\omega_0 t + \angle H(\omega_0)) \quad t \geq 0$$

$$|H(\omega)|_{dB} = 20 \log_{10} |H(\omega)| \quad (= 10 \log_{10} |H(\omega)|^2)$$

↑ power spectrum

Note:

$$|H(\omega)|_{dB} < 0 \text{ dB}$$

if  $|H(\omega)| < 1$  attenuation

$$|H(\omega)|_{dB} = 0 \text{ dB}$$

if  $|H(\omega)| = 1$

$$|H(\omega)|_{dB} > 0 \text{ dB}$$

if  $|H(\omega)| > 1$  amplification

plots of  $|H(\omega)|_{dB}$  vs.  $\omega$   
and  $\angle H(\omega)$  vs.  $\omega$  } → Bode plots. (Bode diagrams.)

↓  
check

11.17.03 Ch 9 Transfer Fun - System Analysis.

First-order case (Single-pole - no zeros)

$$H(s) = \frac{k}{s+B} \rightarrow H(\omega) = \frac{k}{j\omega+B} \quad (= H(s)|_{s=j\omega})$$

$$|H(\omega)| = \frac{k}{\sqrt{\omega^2+B^2}} \quad (|H(\omega)|^2 = H(\omega)\overline{H(\omega)})$$

$$\angle H(\omega) = -\tan^{-1}\left(\frac{\omega}{B}\right)$$

|                    |                         |                                 |                                          |
|--------------------|-------------------------|---------------------------------|------------------------------------------|
|                    | $\omega=0$              | $\omega=B$                      | $\omega \rightarrow \infty$              |
| $H(\omega)$        | $H(0) = k/B$            | $H(B) = k/2B = \frac{1}{2}H(0)$ | $H(\infty) \rightarrow 0$                |
| $\angle H(\omega)$ | $\angle H(0) = 0^\circ$ | $\angle H(B) = -45^\circ$       | $\angle H(\infty) \rightarrow -90^\circ$ |

↑↑  
Characteristics

→ LPF

$\omega < B \rightarrow$  passband  $\therefore$  3dB bandwidth  $= B$  rad/sec.

$\omega > B \rightarrow$  stopband

↑  
3dB point (since  $\frac{1}{2} \rightarrow 3dB$ )

$$|H(B)|_{dB} = |H(0)|_{dB} - 3dB.$$

→ No zero / single pole → poor LPF

— use MATLAB Bode script p. 467

Single-pole / single-zero

$$H(s) = \frac{s+C}{s+B} \rightarrow H(\omega) = \frac{j\omega+C}{j\omega+B}$$

$$|H(\omega)| = \sqrt{\frac{\omega^2+C^2}{\omega^2+B^2}}$$

$$\angle H(j\omega) = \tan^{-1}\left(\frac{\omega}{C}\right) - \tan^{-1}\left(\frac{\omega}{B}\right)$$

$$|H(0)| = \frac{C}{B} \rightarrow |H(\infty)| \rightarrow 1 \quad \omega/C < B \rightarrow \text{HPF.}$$

$$\angle H(0) = 0^\circ \rightarrow \angle H(\infty) \rightarrow 0^\circ$$

↑  
max  $\angle H(\omega)$  occurs  $\forall \omega = C$  and  $\omega = B$ .

skip



# 11-23-03 Ch 9 Transfer Fun. - System Analysis.

## SECOND ORDER SYSTEM.

$$H(s) = \frac{k}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$k > 0, \zeta > 0, \omega_n > 0$ .  
(SYSTEM IS STABLE)

$$= \frac{k}{(s-p_1)(s-p_2)}$$

$$\begin{aligned} w/ p_1 &= -\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1} \\ p_2 &= -\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1} \end{aligned}$$

$$\downarrow$$

$$|H(\omega)| = \frac{k}{|j\omega - p_1||j\omega - p_2|}$$

$$\angle H(\omega) = -\angle j\omega - p_1 - \angle j\omega - p_2 \quad \left\{ \begin{array}{l} p_1, p_2 \text{ are real} \\ \text{iff } \zeta \geq 1 \end{array} \right.$$

$$|H(\omega)|: \omega=0 \quad |H(0)| = \left| \frac{k}{p_1 p_2} \right| = \frac{k}{\omega_n^2} \longrightarrow |H(\infty)| \rightarrow 0$$

$$\angle H(\omega): \angle H(0) = 0^\circ \longrightarrow \angle H(\infty) \rightarrow -180^\circ$$

$$\text{if } k = \omega_n^2 \rightarrow |H(0)| = 1 \rightarrow \text{LPF}$$

$$w/ \zeta = 1 \rightarrow \text{3dB bandwidth} = \sqrt{2^2 - 1} \omega_n$$

$$\text{IF } 0 < \zeta < 1 \rightarrow p_1, p_2 \text{ are complex } w/ p_1, p_2 = -\zeta\omega_n \pm j\omega_d$$

$\Downarrow$

$$\text{where } \omega_d = \omega_n\sqrt{1 - \zeta^2}$$

$$H(\omega) = \frac{k}{(j\omega + \zeta\omega_n + j\omega_d)(j\omega + \zeta\omega_n - j\omega_d)}$$

$$\text{when } \zeta < \frac{1}{\sqrt{2}} \quad |H(\omega)| \text{ increases as } \omega \text{ goes from } 0 \rightarrow \infty \quad |H(\infty)| \rightarrow 0$$

$$\text{when } \zeta \geq \frac{1}{\sqrt{2}} \quad |H(\omega)| \text{ decreases as } \omega \text{ goes from } 0 \rightarrow \infty$$

$$\text{when } \zeta = \frac{1}{\sqrt{2}} \rightarrow \text{RESONANCE. } \omega_r = \omega_n\sqrt{1 - 2\zeta^2} \text{ resonant frequency.}$$

skip

Bode Plot Construction

$$H(s) = \frac{A(s+C_1)(s+C_2)\dots(s+C_M)}{s(s+B_1)(s+B_2)\dots(s+B_{N-1})}$$

zeros @  $-C_1, -C_2, \dots, -C_M$   
poles @  $-B_1, -B_2, \dots, -B_{N-1}$

$$\downarrow$$

$$H(\omega) = \frac{A(j\omega+C_1)(j\omega+C_2)\dots(j\omega+C_M)}{j\omega(j\omega+B_1)(j\omega+B_2)\dots(j\omega+B_{N-1})}$$

$$= \frac{K(j\frac{\omega}{C_1}+1)(j\frac{\omega}{C_2}+1)\dots(j\frac{\omega}{C_M}+1)}{j\omega(j\frac{\omega}{B_1}+1)(j\frac{\omega}{B_2}+1)\dots(j\frac{\omega}{B_{N-1}}+1)}$$

$K = \frac{A C_1 C_2 \dots C_M}{B_1 B_2 \dots B_{N-1}}$

$$\therefore |H(\omega)|_{dB} = 20 \log_{10} |K| + 20 \log_{10} |j\frac{\omega}{C_1}+1| + \dots + 20 \log_{10} |j\frac{\omega}{C_M}+1|$$

$$- 20 \log_{10} |j\omega| - 20 \log_{10} |j\frac{\omega}{B_1}+1| + \dots + 20 \log_{10} |j\frac{\omega}{B_{N-1}}+1|$$

$$\angle H(\omega) = \angle K + \angle(j\frac{\omega}{C_1}+1) + \dots + \angle(j\frac{\omega}{C_M}+1)$$

$$- \angle j\omega - \angle(j\frac{\omega}{B_1}+1) - \dots - \angle(j\frac{\omega}{B_{N-1}}+1)$$

Notes: K:  $|K|_{dB} = 20 \log_{10} |K|$

$$\angle K = 0 \text{ or } 180^\circ$$

$K > 0 \text{ or } K < 0$

$(j\omega T + 1)$ :  $|j\omega T + 1|_{dB} = 20 \log_{10} \sqrt{\omega^2 T^2 + 1}$

if  $\omega_{cf} = \frac{1}{T} \rightarrow \omega_{cf} T = 1$

for  $\omega < \omega_{cf} \rightarrow |j\omega T + 1|_{dB} = 0 \text{ dB}$

for  $\omega > \omega_{cf} \rightarrow |j\omega T + 1|_{dB} = 20 \log_{10} (\omega T)$

Figure 9.25  $\angle(j\omega T + 1) = 0^\circ$  very small frequencies  
 $\angle(j\omega T + 1) = 90^\circ$  very large frequencies

b/w  $0.1\omega_{cf} \neq 10\omega_{cf}$   $\angle(j\omega T + 1)$  increases by  $45^\circ/\text{decade}$

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11.23.03 Ch 9 Transfer Fun - System Analysis

$(j\omega T + 1) \rightarrow$  zeros -  $|j\omega T + 1|_{dB} > 0$   $\angle(j\omega T + 1) > 0$

poles -  $|j\omega T + 1|_{dB} < 0$   $\angle(j\omega T + 1) < 0$

$(j\omega)$  as a zero  $\rightarrow \begin{cases} |j\omega|_{dB} = 20 \log_{10}(\omega) & \text{no breakpoints} \\ \angle(j\omega) = 90^\circ & \text{no shift.} \end{cases}$

as a pole  $\rightarrow \begin{cases} |j\omega|_{dB} = -20 \log_{10}(\omega) \\ \angle(j\omega) = -90^\circ \end{cases}$

Complex poles/zeros  $\rightarrow$  see text

Ch 11 - Z-transform / DTS

$\uparrow$  Discrete Time Systems.  
discrete-time counterpart to Laplace Transform.

Given  $x[n]$

$$\rightarrow \text{DTFT } X(\Omega) = \sum_{n=-\infty}^{\infty} x[n] e^{-j\Omega n}$$

to ensure convergence (absolute summability),  
add  $p^{-n}$  factor as

$$\begin{aligned} X(\Omega) &= \sum_{n=-\infty}^{\infty} x[n] p^{-n} e^{-j\Omega n} \\ &= \sum_{n=-\infty}^{\infty} x[n] (pe^{-j\Omega})^{-n} \end{aligned}$$

let  $z = pe^{-j\Omega}$

$$\rightarrow X(z) = \sum_{n=-\infty}^{\infty} x[n] z^{-n} \quad \text{two-sided}$$

One sided Z transform

$$X(z) = \sum_{n=0}^{\infty} x[n] z^{-n} \quad \text{well-defined if } z \in \text{ROC.}$$

12-01-03 Ch 11 - Z-Transform / DTS

$$X(\Omega) = X(z) \big|_{z=e^{j\Omega}}$$

iff ROC of  $X(z)$  includes  
all complex numbers  $z$

$$\text{s.t. } |z|=1$$

↑  
unit circle  
in complex plane.

### PROPERTIES

Basic relationships

$$\left\{ \begin{array}{l} x[n] = \delta[n] \rightarrow X(z) = 1 \\ x[n] = \delta[n-q] \rightarrow X(z) = z^{-q} \\ x[n] = u[n] \rightarrow X(z) = \frac{z}{z-1} = \frac{1}{1-z^{-1}} \\ x[n] = a^n u[n] \rightarrow X(z) = \frac{z}{z-a} = \frac{1}{1-az^{-1}} \end{array} \right.$$

### LINEARITY

$$ax[n] + bv[n] \rightarrow aX(z) + bV(z)$$

RIGHT SHIFT of  $x[n]u[n]$

$$x[n-q]u[n-q] \rightarrow z^{-q}X(z)$$

RIGHT SHIFT of  $x[n]$

$$x[n-q] \rightarrow z^{-q}X(z) + x[-q] + z^{-1}x[-q+1] + \dots + z^{-q+1}x[-1]$$

$\therefore$  if  $x[n] = 0, n = -1, -2, \dots, -q$

$$\text{then } x[n-q] \rightarrow z^{-q}X(z)$$

LEFT SHIFT of  $x[n]$

$$x[n+q] \rightarrow z^qX(z) - x[0]z^q - x[1]z^{q-1} - \dots - x[q-1]z$$

MULTIPLICATION BY  $n$  &  $n^2$

$$nx[n] \rightarrow -z \frac{d}{dz} X(z)$$

$$n^2x[n] \rightarrow z \frac{d}{dz} X(z) + z^2 \frac{d^2}{dz^2} X(z)$$

12.01.03 Ch 11 z-transform / DTS

MULTIPLICATION BY  $a^n$

$$a^n x[n] \rightarrow X\left(\frac{z}{a}\right)$$

MULTIPLICATION BY  $\cos \Omega n$  &  $\sin \Omega n$

$$x[n] \cos \Omega n \rightarrow \frac{1}{2} [X(e^{j\Omega} z) + X(e^{-j\Omega} z)]$$

$$x[n] \sin \Omega n \rightarrow \frac{1}{2j} [X(e^{j\Omega} z) - X(e^{-j\Omega} z)]$$

SUMMATION

$$v[n] = \sum_{i=0}^n x[i] \rightarrow V(z) = \frac{z}{z-1} X(z)$$

CONVOLUTION

$$x[n] * v[n] \rightarrow X(z) V(z)$$

INITIAL VALUE THEM.

$$x[q] = \lim_{z \rightarrow \infty} [z^q X(z) - z^q x[0] - z^{q-1} x[1] \dots - z x[q-1]]$$

FINAL VALUE THEOREM

$$\lim_{n \rightarrow \infty} x[n] = \lim_{z \rightarrow 1} (z-1) X(z)$$

Inverse z-Transform

$$x[n] = \frac{1}{2\pi j} \int X(z) z^{n-1} dz \quad \text{error in text } (X?)$$

Not generally going to use this form  $\rightarrow$  use PFE.

12-01-03 Ch 11 Z-transform/DTS.

Since  $X(z) = \sum_{n=0}^{\infty} x[n]z^{-n} = x[0] + x[1]z^{-1} + x[2]z^{-2} + \dots$

One way to obtain  $x[n]$  is by long division...

$$X(z) = \frac{B(z)}{A(z)}$$

$A(z), B(z)$  written in descending powers of  $z$  as in

$$\begin{array}{r} X(z) = \frac{z^2 - 1}{z^3 + 2z + 4} \\ \begin{array}{r} z^{-1} + 0z^{-2} - 3z^{-3} - 4z^{-4} \\ z^3 + 0z^2 + 2z + 4 \overline{) z^2 + 0z - 1} \\ \underline{z^2 + 0z + 2 + 4z^{-1}} \\ -3 - 4z^{-1} \\ -3 + 0z^{-1} - 6z^{-2} - 12z^{-3} \\ \underline{-4z^{-1} + 6z^{-2} + 12z^{-3}} \\ -4z^{-4} + 0z^{-2} - 8z^{-3} - 16z^{-4} \\ \underline{6z^{-2} + 20z^{-3} + 16z^{-4}} \\ \vdots \end{array} \end{array}$$

$$\begin{aligned} \therefore x[0] &= 0 \\ x[1] &= 1 \\ x[2] &= 0 \\ x[3] &= -3 \\ x[4] &= -4 \\ &\vdots \end{aligned}$$

Inverse Z-Transform via PFE  $\rightarrow$  If  $\overset{\text{degree of } B(z)}{B(z)} = \overset{\text{degree of } A(z)}{A(z)}$  can't use PFE on  $X(z) = \frac{B(z)}{A(z)}$

$$X(z) = \frac{B(z)}{A(z)} \therefore \left( \begin{array}{l} \text{Note} \\ \text{if degree } B(z) \geq A(z) \rightarrow X(z) = x[0] + \frac{R(z)}{A(z)} \end{array} \right)$$

$\downarrow$  o.w.

$$\frac{X(z)}{z} = \frac{B(z)}{zA(z)}$$

$\swarrow$  can perform PFE on either of these forms

12.02.03 Ch 11. Z-Transform/DTS.

Inverse Z-Transform  $\frac{X(z)}{z}$

DISTINCT POLES poles  $\{p_1, p_2, \dots, p_N\}$  are distinct & non-zero

$$\frac{X(z)}{z} = \frac{c_0}{z} + \frac{c_1}{(z-p_1)} + \frac{c_2}{(z-p_2)} + \dots + \frac{c_N}{(z-p_N)}$$

$$\downarrow$$

$$c_0 = \left[ z \frac{X(z)}{z} \right]_{z=0} = X(0)$$

$$\downarrow$$

$$\{c_i\} = \left\{ \left[ (z-p_i) \frac{X(z)}{z} \right] \right\}_{z=p_i} \quad i=1,2,\dots,N$$

$$X(z) = c_0 + \frac{c_1 z}{z-p_1} + \frac{c_2 z}{z-p_2} + \dots + \frac{c_N z}{z-p_N}$$

$$\downarrow$$

$$X[n] = c_0 \delta[n] + c_1 p_1^n + c_2 p_2^n + \dots + c_N p_N^n \quad n=0,1,2,\dots$$

↑ modes of convergence  
(as in Laplace Transform)

complex poles occur in complex conjugate pairs, s.t.

$c_1 p_1^n + \bar{c}_1 \bar{p}_1^n$  is a term that can be expressed as.

$$2|c_1| \sigma^n \cos(\Omega n + \phi c_1)$$

(remember  $p = \sigma e^{j\Omega}$ )

$$\uparrow$$

$$\sigma = |p|$$

$$\Omega = \angle p$$

12.02.03 Ch 11 - z-Transform / DTS.

REPEATED POLES,  $p_1$  is repeated  $r$  times.

$$\frac{X(z)}{z} = \frac{C_0}{z} + \frac{C_1}{z-p_1} + \frac{C_2}{(z-p_1)^2} + \dots + \frac{C_r}{(z-p_1)^r} + \frac{C_{r+1}}{z-p_{r+1}} + \dots + \frac{C_N}{z-p_N}$$

$$C_r = \left[ (z-p_1)^r \frac{X(z)}{z} \right]_{z=p_1}$$

$$C_{r-1} = \left[ \frac{d}{dz} (z-p_1)^r \frac{X(z)}{z} \right]_{z=p_1}$$

$$\vdots$$

$$C_{r-i} = \frac{1}{i!} \left[ \frac{d^i}{dz^i} (z-p_1)^r \frac{X(z)}{z} \right]_{z=p_1}$$

$$X(z) = C_0 + \frac{C_1 z}{z-p_1} + \frac{C_2 z}{(z-p_1)^2} + \dots + \frac{C_r z}{(z-p_1)^r} + \frac{C_{r+1} z}{z-p_{r+1}} + \dots + \frac{C_N z}{z-p_N}$$

from transform tables,...

$$\frac{C_2 z}{(z-p_1)^2} \rightarrow C_2 n p_1^{n-1} u[n]$$

$$\frac{C_3 z}{(z-p_1)^3} \rightarrow \frac{1}{2} C_3 n(n-1) p_1^{n-2} u[n-1]$$

$$\vdots$$

$$\frac{C_i z}{(z-p_1)^i} \rightarrow \frac{C_i}{(i-1)!} n(n-1)\dots(n-i+2) p_1^{n-i+1} u[n-i+2]$$

In general,  $x[n] \xrightarrow{n \rightarrow \infty} 0$  iff all poles are s.t.  $|p_i| < 1$  for  $i=1, 2, \dots, N$

$x[n] \xrightarrow{n \rightarrow \infty} k$  constant  
iff  $|p_i| < 1$  except one of the  $|p_i| = 1$ .



12.02.03 ch 11 z-transform/DTS.

### TRANSFER FN REPRESENTATION.

First order case (LTI-DTS)

$$y[n] + ay[n-1] = bx[n]$$

$$\downarrow \quad \downarrow$$

$$Y(z) + a[z^{-1}Y(z) + y[-1]] = bX(z)$$

$$(1 + az^{-1})Y(z) = -ay[-1] + bX(z)$$

$$Y(z) = \frac{-ay[-1]}{1 + az^{-1}} + \frac{b}{1 + az^{-1}} X(z)$$

$$= -\frac{ay[-1]z}{z+a} + \frac{bz}{z+a} X(z)$$

if  $y[-1] = 0$  (no initial energy at time  $n=0$ )

$$\text{then } Y(z) = \frac{bz}{z+a} X(z)$$

$$\uparrow H(z) = \frac{bz}{z+a}$$

$$Y(z) = H(z)X(z)$$

Second order case

$$y[n] + a_1y[n-1] + a_2y[n-2] = b_0x[n] + b_1x[n-1]$$

$\downarrow$  if no initial energy, i.e.,  $y[-1] = y[-2] = 0$

$$Y(z) = \frac{b_0z^2 + b_1z}{z^2 + a_1z + a_2} X(z)$$

$$\uparrow H(z) = \frac{b_0z^2 + b_1z}{z^2 + a_1z + a_2}$$

12.03.03 Ch 11 ZTransform/DTS.

$N^{\text{th}}$  Order Case

$$y[n] + \sum_{i=1}^N a_i y[n-i] = \sum_{i=1}^M b_i x[n-i]$$

↓ assuming initial conditions = 0.

$$Y(z) = \frac{b_0 z^N + b_1 z^{N-1} + \dots + b_M z^{N-M}}{z^N + a_1 z^{N-1} + \dots + a_{N-1} z + a_N} X(z)$$



$$H(z)$$

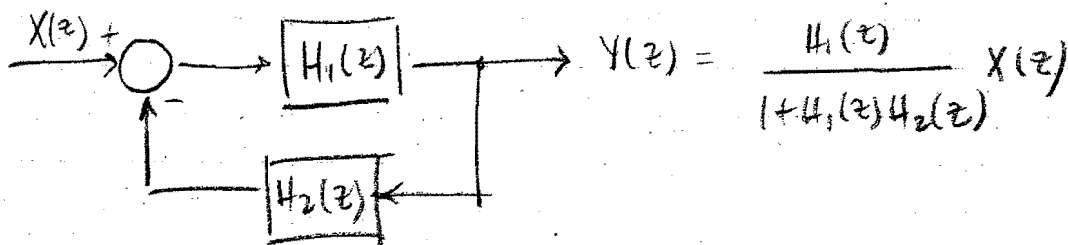
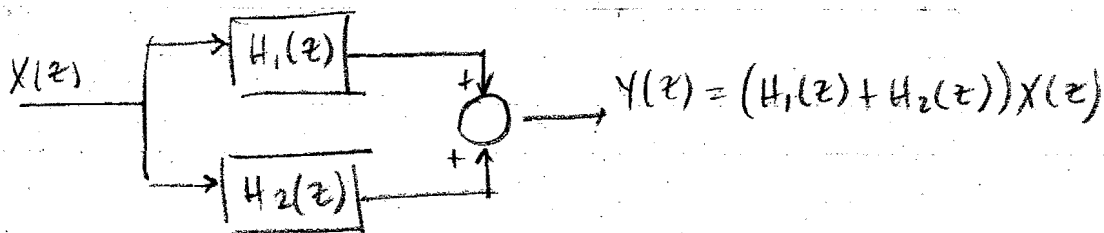
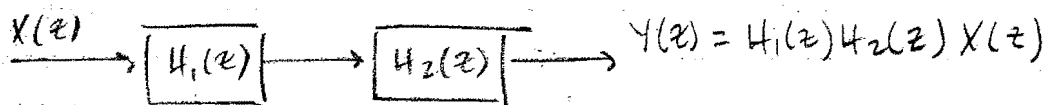
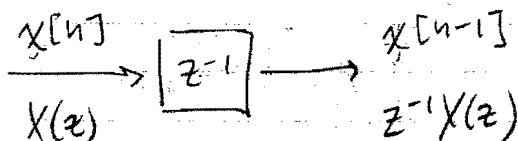


$h[n]$  impulse response

$$Y(z) = H(z) X(z)$$

Transfer fn of Interconnections.

Unit-delay element



# FREQUENCY RESPONSE

$$x[n] = C \cos(\Omega_0 n) \quad n = 0, 1, 2, \dots$$

$$\downarrow$$

$$X(z) = \frac{C[z^2 - (\cos \Omega_0)z]}{z^2 - (2\cos \Omega_0)z + 1}$$

If  $H(z) = B(z)/A(z)$  & no initial energy in system at  $n=0$ ,

then

$$Y(z) = \frac{CB(z)[z^2 - (\cos \Omega_0)z]}{A(z)[z^2 - (2\cos \Omega_0)z + 1]}$$

Note  $H(z) = \frac{B(z)}{A(z)}$   
 $\uparrow$   
assumed STABLE

$$= \frac{CB(z)[z^2 - (\cos \Omega_0)z]}{A(z)(z - e^{j\Omega_0})(z - e^{-j\Omega_0})}$$

$$\therefore \frac{Y(z)}{z} = \frac{\eta(z)}{A(z)} + \frac{C}{z - e^{j\Omega_0}} + \frac{\bar{C}}{z - e^{-j\Omega_0}}$$

$$\downarrow$$

$$C = \frac{C}{2} H(e^{j\Omega_0})$$

$$\Downarrow$$

$$\bar{C} = \frac{C}{2} \overline{H(e^{j\Omega_0})}$$

$$Y(z) = \frac{z\eta(z)}{A(z)} + \frac{C}{2} H(e^{j\Omega_0}) \frac{z}{z - e^{j\Omega_0}} + \frac{C}{2} \overline{H(e^{j\Omega_0})} \frac{z}{z - e^{-j\Omega_0}}$$

$$\uparrow$$

$$y_{tr}[n] \xrightarrow{n \rightarrow \infty} 0 \quad \text{since } H(z) \text{ is assumed stable}$$

$$y_{ss}[n] = C |H(e^{j\Omega_0})| \cos[\Omega_0 n + \angle H(e^{j\Omega_0})]$$

$\uparrow$   
 steady-state output  
 resulting from input  $x[n]$

Since  $H(z)$  is stable,  
 $h[n]$  is absolutely summable

$$\therefore H(\Omega) = H(z) \big|_{z=e^{j\Omega}}$$

$$\therefore y_{ss}[n] = C |H(\Omega_0)| \cos(\Omega_0 n + \angle H(\Omega_0)) \iff$$

$$|H(e^{j\Omega_0})| = |H(\Omega)|_{\Omega=\Omega_0}$$

$$\angle H(e^{j\Omega_0}) = \angle H(\Omega) \big|_{\Omega=\Omega_0}$$